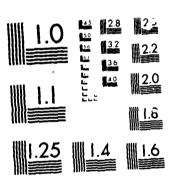
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COMBINED DIRECT/INVERSE THREE DIMENSIONAL TRANSONIC WING DESIGN WITH VISCOUS AND WING/BODY EFFECTS

VOLUME 1: USERS GUIDE FOR ANALYSIS/DESIGN COMPUTER PROGRAM

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Aug. 1984

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Prepared tor

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This Users Guide describes the input and operation requirements of a computer code for the analysis and design of wings in transonic flow. A synopsis of the function of the major subroutines in the program is given in addition to a detailed description of the input variables required to run the code. Sample data sets are presented that illustrate the data sequence required for various code options.

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#### **ABSTRACT**

This users guide describes the input and operation requirements of a computer code for the analysis and design of wings in transonic flow. A synopsis of the function of the major subroutines in the program is given in addition to a detailed description of the input variables required to run the code. Sample data sets are presented that illustrate the data sequence required for various code options.

#### ADMINISTRATIVE INFORMATION

The work presented was a joint effort by Lockheed-Georgia Company and Texas ASM University supported by the Naval Air Systems Command under the cognizance of D. G. Kirkpatrick (NAVAIR-311D AIRTASK WR02302), Navy Contract N00167-81-C-0078-P00004. The authors acknowledges the support of Dr. Tsze C. Tai, contract monitor at David Taylor Ship/Research and Development Center during all phases of this research.

#### INTRODUCTION

This users guide describes the inputs required to run the Lockheed-Georgia Direct/Inverse Design Code (ZEBINV) in the analysis and design modes. The following sections include a brief description of how the code works, a detailed description of the required input data, along with sample input decks and an example of the typical output from the code.

#### DESCRIPTION OF CODE OPERATION

In the analysis mode, the Lockheed Georgia Direct/Inverse Design Code (ZEBINV) computes the inviscid potential flow about three-dimensional wings using the ZEBRA II algorithm developed by South et al<sup>1</sup>. The conservative full potential equation is solved on a stretched Cartesian grid that is sheared to align with the leading and trailing edges of the wing.

A typical analysis run begins with the inputting of data that define the airfoil geometry at different spanwise control stations, the wing planform geometry, mesh generation parameters, flow solver initialization and control

parameters. Subroutines SECTIN and INPUT control the reading in of all analysis data. After the required data has been input, the program calls routines to generate the computational grid (SETUP) and compute initial flow parameters (INIT). Subroutine ZEBRA is then called to generate the potential flow solution. ZEBRA calls subroutine WNGBC2 to compute and update both wing surface and outer grid boundary condition, subroutine RO to compute the density at grid half points, and subroutine ROCOZ to compute the retarded density coefficients used in the potential flow solver. Subroutine OUTPUT is called at the end of the solution to compute and print output parameters.

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When viscous analysis or design is selected, subroutine VISACT is called from ZEBRA to compute the displacement thickness due to the boundary layer and to update the surface boundary conditions to account for the viscous effects. A second viscous flow routine BDLY is called to compute viscous effects during inverse design cases.

Wing/body effects are computed in subroutine WONZ which is called by INIT. WONZ is called prior to the start of the potential flow solution for each grid of a grid sequencing run.

During inverse design cases, two subroutines are called to compute the current wing shape and perform a wing reloft to enforce a desired trailing edge thickness. These subroutines are SHAPE and RELOFT. When relofting is in effect SHAPE is called by RELOFT. RELOFT is called from subroutine ZEBRA at a specified iteration frequency.

The sequencing of the input routines, flow solver, and output routines is controlled by the main program ZEBINV. This program contains logic that allows grid sequencing to be used to speed up the flow solution. The sample data sets presented in the following sections illustrate the use of a sequence of three grids in the flow solution.

# DETAILED DESCRIPTION OF INPUT

The input data set required by the analysis/design code can be

broken into five distinct types of data. These data types are:

- 1. Airfoil section ordinates at specified span locations
- 2. Data to define the wing planform
- 3. Control parameters for mesh generation and solution initial
- 4. Wing/Body data

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5. Inverse design data

Each different type of data will be described separately. The input be described card by card. This description will contain both definition of the input variable and the input format.

## A. Airfoil Section Inputs and Test Case Title

Section ordinates can be defined at up to 11 span locations of the airfoil section ordinates are:

1. TITLE1, TITLE2, ATITLE (3 cards, 8A10)

TITLE1 - Two card test case title and description that

TITLE2 is written to output files.

ATITLE - Airfoil data description.

# 2. NPAN, INU, INL, KSMTHS (1 card, 8110)

NPAN - Number of span stations at which airfoil ordinates are to be defined - at least two stations are required (2.LE.NPAN.LE.11)

> INU = Number of upper surface airfoil ordinates. Must be the same for all sections .LE. 100.

> INL = Number of lower surface airfoil ordinates. Must be

the same for all sections .LE. 100.

KSMTHS = Number of times computed surface slopes are smoothed.

- XINU(I), I = 1, INU (INU/8 Cards, 8F10.0) x/c at which airfoil upper surface ordinates are input for the wing section.
- 4. XINL(I), I = 1, INL (INL/8 Cards, %F10.0) x/c at which air-foil lower surface ordinates are input for the wing section.
- 5. ZUP(I, 1), I = 1, INU (INU/8 Cards, 8F10.0) upper surface airfoil ordinates (Z/C) at wing root.
- 6. ZLP(I, 1) I = 1, INL (INL/8 Cards, 8F10.0) lower surface airfoil ordinates at the wing root station.

The airfoil sections at span stations 2 through NPAN are defined by the following sequence of cards.

- 7. ISAMX, ISAMZ (1 Card, 2L5).
  - ISAMX = T ordinates will be defined at the x/c locations of
     the root section.
    - = F new x/c locations will be input. The corresponding z/c ordinates will then be splined onto the root X/C locations.
  - ISAMZ = T use ordinates for previously defined station.
    - = F input new z/c ordinates.
- 8. If ISAMX = T AND ISAMZ = F, repeat cards 5 and 6 after 7.
- 9. If ISAMX = F and ISAMZ = F, repeat cards 3 through 6 after card 7.

10. To use airfoil section defined at station N-1 at station N, repeat card 7 with ISAMX = T and ISAMZ = T.

## Planform Geometry

- 1. Header (2X)
- 2. PTITLE (1 Card, 8A10)

80 character wing planform description

3. YROOT, XLER, XTER, YTIP, XLET, XTET, SREF, CREF, YMON (2 Cards, 5F10.0)

These variables define trapezoidal reference wing:

YROOT = Y coordinate of root

XLER = X coordinate of L.E. at root

XTER = X coordinate of T.E. at root

YTIP = Y coordinate of tip

XLET = X coordinate of L.E. at tip

XTET = X coordinate of T.E. at tip

SREF = Wing reference area (Semi Span Area)

CREF = Reference chord

XMON = Moment reference

4. NLES (1 Card, 8110)

NLES - Number of segments input to describe the leading edge (NLES.LE.3).

5. NLEI (1 Card, 8110)

NLEI = Number of Y,X pairs defining leading edge (NLEI.LE.10).

6. YLEI(I), XLEI(I), I=1, NLEI (NLEI/4 Cards, 8F10.0)

YLEI, XLEI = Y, X pairs defining the leading edge segment

At least two pairs required.

Same dimensional system as XLER, etc.

". DXLER, DXLET (1 Card, 8F10.0).

DXLER = DX/DY of L.E. at inboard edge of segment

DXLET = DX/DY of L.E. at outboard edge of segment

Note: Repeat cards 5 through 7 NLES times

8. NTES (1 Card, 8110)

NTES = Number of segments input to describe the trailing edge (NTES.LE.3)

9. NTEI (1 Card, 8110)

NTEI = Number of Y,X pairs defining trailing edge segment
(NTEI.LE.10).

10. YTEI(1), XTEI(1), I=1, NTEI (NTEI/4 Cards, 8F10.0)

YTEI,XTEI = Y,X pairs defining the trailing edge segment

At least two pairs required

11. DXTER, DXTET (1 Card, 8F10.0)

DXTER = DX/DY of T.E. at inboard edge of segment

DXTET = DX/DY of T.E. at outboard edge of segment

NOTE: Repeat cards 9 through 11 NTES times

12. YP(N), THETP(N), N=1, NPAN (NPAN/4 Cards, 8F10.0)

YP = Fraction of semispan at which airfoils are defined

THETP = Twist Angle, degrees, at YP - Positive if leading edge is up

# C. Mesh Generation and Solution Parameters

A set of five namelists are used to input values that control mesh generation, solution initialization and solution sequencing. Namelist GPARM, XGRID, YGRID, and ZGRID are used in mesh generation. Namelist SOLVIN is used to put flow solver parameters. A sixth namelist VISCDT is input after SOLVIN if IVISC = 1 in SOLVIN. This set of namelists must be input for each grid in a grid sequencing run; however, only those values that change from grid to grid must be redefined. The namelists and the input parameters required for analysis runs are:

- 1. TITLEM (1 Card, 8A10)

  Namelist set description
- GPARM (Namelist input Default values in parenthesis)

IPRNTG = 1 - Prints computational grid (0)

WBCPRT = .T. - Prints upper and lower surface slopes at each
spanwise grid station (.F.)

NTIPLE = 1 - Generates a constant chord tip extension with tip section sweep from wing tip to outer boundary

#### 3. XGRID (Namelist input)

- NXON Number of streamwise mesh points on wing surface at each span station
- NXFWD- Number of streamwise mesh points ahead of the wing leading edge
- NXAFT- Number of streamwise mesh points aft of the wing trailing edge
- XPLE Grid stretching factor for grid in front of wing; computed in MESHZ for XFWD .NE.0
- XPTE Grid stretching factor for grid behind wing; computed in MESH? for XAFT .NE.O
- XFWD Desired location of the upstream boundary referenced to the leading edge of the wing (in root chords).
- XAFT Desired location of the downstream boundary referenced to the leading edge of the wing (in root chords).

## 4. YGRID (Namelist input)

- NYON Number of spanwise grid points on wing surface
- NYOFF- Number of spanwise grid points off of the wing surface
- YPTIP- Grid stretching factor for grid beyond wing tip, computed in MESHZ when YMAX .NE.0

YMAX - Desired location of the spanwise outer boundary referenced to the wing tip (in semi-spans). For example, YMAX=1.3 places the spanwise boundary at 1.3 semi-spans beyond the wing tip.

#### 5. 2GRID (Namelist input)

NZ - Number of vertical grid points

ZP - Grid stretching factor for vertical direction. The grid is stretched equally above and below the z = 0 plane.
Computed in MESHZ when ZMAX .NE.0

ZMAX - Desired location of the top and bottom boundaries of the computational plane (in root chords).

# 6. SOLVIN (Namelist input)

MACH - Free-stream Mach number for test case

AOA - Wing angle of attack in degrees

OMEGX

OMEGY- Relaxation parameters for the x, y, and z directions OMEGZ

OMEGG- Relaxation factor for circulation

MAXIT- Maximum number of iterations of the flow solver

RCONV- Convergence tolerence = the ratio of current maximum residual and initial residual

NGSEQ- Number of grids to be used in grid sequencing runs

IPRINT = 1 - Calls output to print flow solution parameters

- IVISC = 1 Selects viscous analysis/design mode
- IFUSE = 1 Turn on wind body effects with circular cylinder fuselage
  - = 2 Turn on wing body effects using input fuselage cross-sections
- ICIRPF Spanwise circulation distribution print frequency Prints every ICIRPF iterations
- - = 0 Sets outer boundary potentials to zero
- IPU Logical unit to which plot data will be written
- IINV = 1 Perform inverse design
- IDESN = 1 Design both upper and lower surfaces
  - = 2 Design upper surface only
  - = 3 Design lower surface only
- IRLOFT = 1 Start wing relofting for trailing edge closure on initial
   grid for NGSEQ.NE.0
  - = 2 Start wing relofting for trailing edge closure on second grid for NGSEQ.NE.O.
  - = 3 Start wing relofting for trailing edge closure on third grid for NGSEQ.NE.0.

NF - Number of fuselage control points used to evaluate wing/body effects (50 or less)

NITRL - Perform NITRL iterations before first wing reloft

NITRF - Reloft wing every NITRF iterations

NJSHP - Print relofted data every NJSHP span stations

NITDSN - Perform NITDSN iterations prior to start of inverse design

ILED - Initial chordwise index to begin inverse design

ITED - Trailing edge index

ISVSHP - Save inverse shapes at end of run

IRSTRT - Restart from previous run

ISRLOR - Save relofted ordinates for restart runs

IPRSHP - Print relofted shapes

7. VISCOT (Namelist input) - only if IVISC .NE. 0 in SOLVIN

RN - Reynolds number based on root chord

DELCOR - Square of the cosine of an appropriate sweep angle such as the mid-chord used to modify boundary layer calculation for 3D effects

NVISC - Number of potential flow solver iterations prior to first viscous update

- ITR Updates viscous corrections every ITR iterations after first update
- NPRV Print viscous flow information every NPRV iterations
- NJPRV Print viscous information every NJPRV span stations
- XIBDLY X/C location of transition point for both upper and lower surfaces
- XSEP X/C location before which the seperation parameter, SEP, is restricted to a maximum value of 0.004. After XSEP, SEP can have any value
- XPCI Lower surface X/C location after which a decreasing lower surface displacement thickness is forced to continue decreasing

#### D. Wing/body Data

The format of the wing/body data depends on the value of IFUSE entered in namelist SOLVIN. If IFUSE = 1, the fuselage is simulated by a circular cylinder with elliptic end caps. If IFUSE=2, the cross-sectional areas of the fuselage are input, see sample cases 4 and 5. The wing/body input is performed only once during a grid sequencing run, usually a call to SOLVIN.

The input sequence for the wing/body data is:

- 1. Header card (1%)
- 2. XBOD, YBOD, ZBOD, RBOD, TL, ALF (8F10.6)
  - XBOD Distance from nose of fuselage to leading edge of wing at the wing root
  - YBOD Distance from centerline of the body to the wing root

ZBOD - Distance from centerline of the body to the centerline of the wing (positive is up)

RBOD - Radius of circular cylinder body for IFUSE = 1

TL - Length of the fuselage

ALF - Length of semimajor axis of ellipsoidal ends for IFUSE=1

if IFUSE = 2, input:

- 3. Header card (1X)
- 4. NST Number of cross-sections to be input (I5)
- 5. XFL(I), AREA(I), I=1, NST (8F10.6)

XLF - % Fuselage length

AREA - Cross-sectional area at XFL

## E. Inverse Design Input

When IINV=1 in SOLVIN, the target pressure distribution for the specified span stations must be input. If IDESN=1, the target pressures for both the upper and lower surfaces are input. If IDESN = 2 or 3, the target pressures for either the upper or the lower surface are input. The card sequence for the inverse design input is as follows; see sample data set 6:

- 1. Header card (1X)
- 2. JD1, JD2, NCPS (315)

JD' - Index of initial spanwise inverse design station

- JD2 Index of final spanwise design station
- NCPS Number of chordwise points in the target pressure distribution
- 4. CPDU(J,I), I=1,NCPS Lower surface target Cp values (7F10.6)
- 5. XLD(J,I), I=1,NCPS Lower surface target Cp X/C locations (7F10.6)
- 6. CPDL(J, I), I=1,NCPS Lower surface target Cp values (7F10.6)

Repeat cards 3 through 6 for J=JD1,JD2

Omit cards 5 and 6 for IDESN=2

Omit cards 3 and 4 for IDESN=3

If relofting (IRLOFT .GT. 0) is selected for either viscous or inviscid design cases, the desired trailing edge ordinates of the surface being designed is input after the target pressure data. The card sequence for the relofting data is as follows:

- 1. Header card (1%)
- 2. NTE Number of relofting stations input. This should be equal to the number of design stations (I5)
- ZUTED(I) ,I=JD1,JD2 Desired upper surface ordinate of design airfoil. (7F10.0)
- 4. ZLTED(I) , I=JD1, JD2 Desired lower surface ordinate of design

#### airfoil. (7F10.0)

Omit cards 4 for IDESN=2.

Omit cards 3 for IDESN=3.

#### DESCRIPTION OF OUTPUT

#### PRINTED OUTPUT

WARRY WARRY WARRY

A typical output will have three sections. In the first section, the parameters that were input to define the wing geometry are echoed. The x location of the wing leading and trailing edges and slope of the leading edge and trailing edge lines at different span stations are printed along with the computed planform geometry parameters such as aspect ratio and taper ratio. These values are normalized by the root chord. The next section of data is generated during the solution process. At the end of each iteration, the iteration number, the grid indicies and values of the maximum correction and residual, the number of supersonic points, the current wing lift coefficient based on circulation and the average residual are printed. If IPRINT = 1 subroutine OUTPUT will be called to compute and print the section lift drag, and moment coefficients and the chordwise upper surface pressure coefficient, density and mach number and lower distributions at each spanwise grid station. A printer plot of the pressure coefficients is also generated.

During inverse runs the relofted shape is printed every NSHPF iterations. If relofting has been selected, the correction to the trailing edge thickness applied at each design station is printed.

When viscous analysis or design is selected, a summary of the boundary layer parameters are printed everyd NPRV updates of the boundary layer for both the upper and lower surfaces of the wing. In addition, a summary of the trailing edge displacement thickness at each wing station is printed every time the boundary layer is recalculated along with the computed skin

friction coefficient. The boundary layer summary includes printout of the local Reynolds number used in the boundary layer calculation, the local Mach number, the displacement thickness, the momentum thickness, and the separation index. A printer plot of wing sections before and after application of the displacement thickness is also printed every NPRV iterations.

#### MASS STORAGE OUTPUT

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When the IPLOT flag is set, the program will output data to mass storage for plotting or other post-processing. The majority of data written to mass storage will be stored on logical unit 3. However, additional data will be stored on other units for design or viscous analysis runs. The definitions of these data are discussed in the following sections. The order and format of the data can be obtained from a listing of subroutine PLTOUT.

## Data Stored on Logical Unit 8

TITLE1 - Test case title and description from input

TITLE2 - Test case title and description from input

MACH - Freestream mach number

AOA - Wing angle of attack

CLW - Computed wing lift coefficient

CDW - Computed wing drag coefficient

CMW - Computed wing pitching moment coefficient

CLG - Wing circulation lift coefficient

SREF - Wing reference area

CROOT - Wing root chord length

SPAN - Wing semi-span length

AR - Wing aspect ratio

JTPM1 - Number of chordwise computational grid planes on the wing

IDUM - Dummy integer

J - Index of chordwise grid plane along semi-span

ETA - Spanwise distance of grid plane J from the root normalized by the semi-span.

XLEW - X coordinate of wing leading edge on grid plane J

XTEW - X coordinate of wing trailing edge on grid plane J

CORDW - Local wing chord at grid plane J

NXB - Number of chordwise grid points on wing at grid plane J

JTIP - Index of the first grid plane off of the wing

YTIP - Eta location of the wing tip

XLET - X coordinate of the wing tip leading edge

XTET - X coordinate of the wing tip trailing edge

CTIP - Wing tip chord

XIN - X/C location of computed data

CPL - Lower surface pressure coefficient

- CPU Upper surface pressure coefficient
- CLS Sectional lift coefficient at grid plane J
- CDS Sectional drag coefficient at grid plane J
- CMS Sectional moment coefficient at grid plane J
- TWIST Twist angle of airfoil section at grid plane J
- ZOCU Wing section upper surface ordinates at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.
- ZOCL Wing section lower surface ordinates at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.
- DZXU Wing section upper surface slopes at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.
- DZXL ~ Wing section lower surface slopes at computational grid X/C's. For viscous analysis and design these values will be for the fluid airfoil.
- INU Number of chordwise points used to define initial airfoil section upper surface.
- INL Number of chordwise points used to define initial airfoil section lower surface.

アンス 動物では アンスク 法権 アンス・スペンド 関ラ インファンス は 見た かっかた たいほ

ZUPI - Airfoil section upper surface ordinates interpolated from the original input airfoil sections. ZUPI will change if relofting is used in design runs.

- ZLPI Airfoil section lower surface ordinates interpolated from original input airfoil sections. ZLPI will change if relofting is used in design runs.
- ITCNT Total number of iterations on all grids used in solution.
- NSPT The number of supersonic points at a given iteration.
- CLGT The circulation lift at a given iteration.
- RMAXT The maximum residual at a given iteration.
- CMAXT The maximum correction at a given iteration.
- ZINU X/C location of input airfoil upper surface ordinates.
- XINL X/C location of input airfoil lower surface ordinates.
- XINUS Initial values of XINU saved when IDESN .NE. O.
- XINLS Initial values of XINL saved when IDESN .NE. O.
- ZUPS Initial values of ZUPI saved when IDESN .NE. O.
- ZLPS Initial values of ZLPI saved when IDESN .NE. O.
- Data Stored on Logical Unit 9 when ISVSHP .NE. 0.
  - TITLE1 Test case title and description from input
  - NJD Total number of inverse design stations
  - ETA Spanwise distance of grid plane J from the root normalized by the semi-span.

NXB - Number of chordwise grid points on wing at grid plane J

XIN - X/C location of computed data

Data Stored on Logical Unit 20 when IVISC .NE. 0.

TITLE1 - Test case title and description from input

JTPM1 - Number of chordwise computational grid planes on the wing

NXB - Number of chordwise grid points on wing at grid plane J

XIN - X/C location of computed data

DPUOLD - Upper surface boundary layer displacement thickness

DPLOLD - Lower surface boundary layer displacement thickness

#### RESTART DATA

Data to restart either an analysis or design case from a previous run is stored on units 7 and 14 by subroutine SAVSOL. At the end of each case, the computational grid, reduced potential and circulation are stored in unformatted form on logical unit 7. For inverse design cases, the relofted ordinates resulting from the design are stored on logical unit 14 whenever ISRLOR .NE. O.

# APPENDIX A SAMPLE DATA SETS

The following sample data sets were used in the evaluation of the direct/inverse design method.

# SAMPLE DATA SET NO. 1 ONERA M6 VISCOUS INVERSE AT J=12

M6 VISCOUS INVERSE AT ONE STATION (J=12) USEING MODIFIED CP'S MACH=0.8395 AOA=3.06 ONERA M6 ORDINATES- 50X30X30

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                          69
                                     0
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          0.000323 0.000551 0.000866
                                        0.001287
                                                 0.001836
                                                            0.002544
                                                                      0.003443
0.004570
          0.005975 0.007711
                              0.009841
                                        0.012448
                                                 0.015617
                                                            0.019461
                                                                      0.024107
                             0.054125
0.029701
          0.036426
                    0.044485
                                        0.065630
                                                  0.079337
                                                            0.095635
                                                                      0.114980
          0.164998 0.191933
                             0.218710 0.245331
                                                  0.271798
 0.137896
                                                            0.298111
                                                                      0.324273
0.350283
          0.376145 0.401857 0.427422 0.452844
                                                 0.478120
                                                            0.503251
                                                                      0.528243
 0.553094
          0.577804 0.602376 0.626810 0.651109
                                                  0.675273
                                                            0.699303
                                                                      0.723199
 0.746966
          0.770600
                    0.794106
                              0.817483 0.840732
                                                  0.863856
                                                            0.886823
                                                                      0.906191
 0.922534
          0.936335
                              0.957851
                                                            0.979202
                    0.947995
                                        0.966186
                                                  0.973236
                                                                      0.984251
 3.988525
          0.992144
                    0.995208
                              0.997803
                                        1.000000
0.000000
          0.000323
                    0.000551 0.000866 0.001287
                                                 0.001836
                                                            0.002544
                                                                      0.003443
 0.004570
          0.005975
                    0.007711 0.009841
                                        0.012448 0.015617
                                                            0.019461
                                                                      0.024107
 0.029701
          0.036426
                    0.044485 0.054125 0.065630
                                                  0.079337
                                                            0.095635
                                                                      0.114980
 0.137896
          0.164998
                    0.191933
                              0.218710 0.245331
                                                 0.271798
                                                            0.298111
                                                                      0.324273
 0.350283
          0.376145
                    0.401857
                              0.427422
                                        0.452844
                                                  0.478120
                                                            0.503251
                                                                      0.528243
0.553094
          0.577804
                    0.602376 0.626810 0.651109
                                                 0.675273
                                                            0.699303
                                                                      0.723199
 0.746966
          0.770600
                    0.794106 0.817483 0.840732
                                                 0.863856
                                                            0.886823
                                                                      0.906191
0.922534
          0.936335
                    0.947995 0.957851
                                        0.966186
                                                  0.973236
                                                            0.979202
 0.988525
          0.992144
                    0.995208
                              0.997803
                                        1.000000
 0.000000 0.003138
                    0.004096 0.005134
                                        0.006260
                                                 0.007478
                                                            0.008796
                                                                      0.010216
          0.013371
                                                 0.020622
0.011742
                    0.015095 0.016898
                                        0.018754
                                                            0.022455
                                                                      0.024200
0.025825
          0.027332 0.028791 0.030328 0.032014
                                                 0.033837
                                                            0.035774
                                                                      0.037792
0.039852
          0.041909
                    0.043621 0.045051
                                        0.046236 0.047199
                                                            0.047949
                                                                      0.048490
 0.048818
          0.048930
                    0.048820 0.048483 0.047935
                                                  0.047166
                                                            0.046190
                                                                      0.045021
0.043674
          0.042168
                    0.040524 0.038761
                                        0.036899
                                                            0.032940
                                                  0.034954
                                                                      0.030866
0.028737
          0.026550 0.024303 0.021984
                                        0.019584
                                                  0.017091
                                                            0.014505
                                                                      0.012239
0.010273 0.008583 0.007142 0.005922 0.004891
                                                 0.004018 0.003280 0.002655
0.002126 0.001678 0.001298 0.000977 0.000705
0.000000 - 0.003138 - 0.004096 - 0.005134 - 0.006260 - 0.007478 - 0.008796 - 0.010216
-0.011742 -0.013371 -0.015095 -0.016898 -0.018754 -0.020622 -0.022455 -0.024200
-0.025825 \ -0.027332 \ -0.028791 \ -0.030328 \ -0.032014 \ -0.033837 \ -0.035774 \ -0.037792
-0.039852 -0.041909 -0.043621 -0.045051 -0.046236 -0.047199 -0.047949 -0.048490
-0.048818 -0.048930 -0.048820 -0.048483 -0.047935 -0.047166 -0.046190 -0.045021
-0.043674 -0.042168 -0.040524 -0.038761 -0.036899 -0.034954 -0.032940 -0.030866
-0.028737 -0.026550 -0.024303 -0.021984 -0.019584 -0.017091 -0.014505 -0.012239
-0.010273 -0.008583 -0.007142 -0.005922 -0.004891 -0.004018 -0.003280 -0.002655
-0.002126 -0.001678 -0.001298 -0.000977 -0.000705
```

T T T T T

```
**** END OF SECTION DATA ****
              ONERA M6 PLANFORM DESCRIPTION
                    805.9
          0.0
                              1196.3
                                        690.68413 1143.5999
752960.07 646.07
                    201.475
         1
         2
                    1196.3
          0.0
                               690.68413
.57735027 .57735027
         1
         2
0.0
          805.9
                    1196.3
                               1143.5999
.28297148 .28297148
                    .20000
                              0.0
                                         .60000
                                                   0.0
                                                              .99999
                                                                          0.0
          0.0
COARSE SKEWED MESH
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0, NTIPLE=1&END
&XGRID NXON=10, NXFWD=7, NXAFT=8, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=1.3&END
 &ZGRID NZ=8, ZP=3.655, &END
 &SOLVIN MACH=0.8395,AOA=3.06,MAXIT=200,OMEGX=1.92,
         OMEGY=1.92, OMEGZ=1.92, RCONV=.00001,
         CON=1.0, NGSEQ=3, BXI=0.0, IPRINT=0, ICIRPF=100,
         IPLOT=0, IPU=8, OMEGG=1.2, IKLUNK=1, IDESN=0&END
MEDIUM SKEVED MESH
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0&END
 &XGRID NXON=25, NXFWD=10, NXAFT=10, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=1.3&END
 &ZGRID NZ=16,ZMAX=5.0&END
 &SOLVIN MAXIT=400, OMEGX=1.95,
         OMEGY=1.95,RCONV=.0001,IPRINT=0,ICIRPF=400,IVISC=1,NITRL=100,
         OMEGZ=1.95, CON=1.0, BXI=0.0, NDIF=0, IRLOFT=3, NITRF=10,
         IPLOT=0, IPU=8, OMEGG=1.2, IKLUNK=1, IDESN=2, ILED=16,
         ITED=35, NITDSN=50, ISVSHP=1, IINV=1&END
 &VISCDT ITR=10, NVISC=50, NPRV=401, NJPRV=9, RN=25000000..DELCOR=.844&END
  ONERA M6 INVERSE WITH CP MODS
   12
        12
             50
   .010101
             .030303
                                  .070707
                        .050505
                                            .090909
                                                      .111111
                                                                 .131313
   .151515
             .171717
                        .191919
                                  .212121
                                            .232323
                                                      .252525
                                                                 .272727
   .292929
             .313131
                                  .353535
                       .333333
                                            .373737
                                                      .393939
                                                                 .414141
   .434343
             . 454545
                       .474747
                                  .494949
                                            .515152
                                                      .535354
                                                                 .555556
   .575758
             .595960
                       .616162
                                  .636364
                                            .656566
                                                      .676768
                                                                 .696970
   .717172
             .737374
                        .757576
                                  .777778
                                            .797980
                                                      .818182
                                                                 .838384
   .858586
             .878788
                        .898990
                                  .919192
                                            .939394
                                                      .959596
                                                                 .979798
  1.000000
  -.346519 -1.127327 -1.172505 -1.109415 -.985884
                                                    -.830017
                                                               -.676677
  -.569370 -.524577 -.521298 -.535000 -.535000 -.535000 -.535000
  -.535000 -.535000 -.535000 -.535000 -.535000 -.535000
  -.535000 -.535000 -.535000 -.525000 -.515000
                                                    -.465000 -.395000
  -.310000
           -.210000 -.160000 -.149000 -.139435
                                                     -.126411
                                                               -.112294
  -.097759 -.083227 -.068499 -.053475 -.037875 -.020879
```

```
.020060
            .045692
                       .075811
                                 .111197
                                            .152444
                                                       .200354
                                                                 .260610
  .347980
TRAILING EDGE THICKNESS TARGETS
   1
0.01
FINE SKEWED MESH
&GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0&END
&XGRID NXON=50, NXFWD=20, NXAFT=20, XFWD=-5.0, XAFT=8.0&END
&YGRID NYON=20,NYOFF=10,YMAX=1.3&END
&ZGRID NZ=30,ZMAX=5.0&END
&SOLVIN MAXIT=400, OMEGX=1.85, OMEGY=1.85, OMEGZ=1.85,
        RCONV=.001, IPRINT=1, ICIRPF=400, NITRL=100, NITRF=10,
        IPLOT=1, IPU=8, OMEGG=1.2, IKLUNK=1, IPRSHP=0, ISRLOR=1,
        NJSHP=1,BXI=0.0,CON=1.0,ILED=31,ITED=70,NITDSN=1,IVISC=1&END
&VISCDT ITR=10, NVISC=50, NPRV=400, NJPRV=9, RN=25000000., DELCOR=.844&END
```

#### SAMPLE DATA SET NO. 2 C5 INVISCID DESIGN AT J=1-19

C5 INVISCID INVERSE TEST CASE DESIGN STATIONS J=1-19 MACH=0.775 AOA=2.0

```
C5 ORDINATES
        5
                          31
                                     0
                 31
 0.000000 0.002500 0.005000 0.007500 0.010000 0.020000 0.040000
                                                                    0.060000
 0.080000
           0.100000
                     0.120000
                              0.140000 0.160000 0.180000 0.200000
                                                                    0.250000
 0.300000
           0.350000
                    0.400000
                              0.450000 0.500000 0.550000 0.600000
                                                                    0.650000
                                                          1.000000
 0.700000
           0.750000
                    0.800000
                              0.850000 0.900000 0.950000
                                                           0.040000
 0.000000 0.002500
                    0.005000
                              0.007500
                                       0.010000 0.020000
                                                                    0.060000
 0.080000 0.100000 0.120000 0.140000 0.160000 0.180000
                                                           0.200000
                                                                    0.250000
 0.300000 0.350000
                    0.400000
                              0.450000
                                       0.500000 0.550000
                                                           0.600000
                                                                    0.650000
 0.700000 0.750000 0.800000 0.850000 0.900000 0.950000
                                                          1.000000
 0.005629
          0.033540
                                                                    0.039428
 0.043911 0.047641
                     0.050505 0.053343 0.055845
                                                 0.057955
                                                           0.060064
                                                                    0.063924
 0.066743 0.068500 0.069185 0.069162 0.067669 0.065596 0.062679
                                                                    0.059085
 0.054549 0.049070 0.042514 0.034879 0.025692 0.014690 0.001289
 0.005629 - 0.004190 - 0.007038 - 0.008982 - 0.010615 - 0.015610 - 0.023116 - 0.029223
 -0.034191 -0.038352 -0.041568 -0.044785 -0.047620 -0.050058 -0.052488 -0.056812
 -0.059852 \ -0.061615 \ -0.062032 \ -0.061170 \ -0.059031 \ -0.055746 \ -0.051383 \ -0.045872
 -0.039654 -0.032971 -0.025789 -0.018461 -0.011621 -0.005749 -0.001289
 0.005809 0.011672 0.014924 0.017571 0.019632 0.026053 0.033823
                                                                    0.039802
 0.044405 0.048000 0.051196 0.054105 0.056622 0.058782 0.060932
                                                                    0.064926
 0.067822 0.069720 0.070620 0.070620 0.069721 0.067824 0.065028
                                                                    0.061433
 0.056841 0.051152 0.044167 0.035851 0.025811 0.014433 0.001102
 0.005809 \ -0.003927 \ -0.007067 \ -0.009012 \ -0.010608 \ -0.015152 \ -0.021136 \ -0.025732
 -0.029260 -0.032049 -0.034070 -0.036030 -0.037737 -0.039097 -0.040457 -0.042838
 -0.044252 -0.044963 -0.044878 -0.044076 -0.042477 -0.040179 -0.037182 -0.033486
 -0.029001 -0.024299 -0.019404 -0.014604 -0.009811 -0.005317 -0.001102
    F
 0.005803 0.011569 0.014967 0.017536 0.019638 0.026077 0.033879 0.039897
 0.044300 0.047900 0.051409 0.054366 0.056903 0.059081 0.061220
                                                                    0.065323
 0.06824_ 0.070083 0.071061 0.071169 0.070280 0.068432 0.065714
                                                                    0.062026
 0.057580 0.051847 0.044714 0.035995 0.025915 0.013754 0.001094
 0.005803 -0.003995 -0.007043 -0.008954 -0.010571 -0.014972 -0.020606 -0.024799
 -0.027976 -0.030345 -0.032038 -0.033668 -0.035028 -0.036028 -0.037028 -0.038832
 -0.039827 -0.040179 -0.039969 -0.039203 -0.037795 -0.035693 -0.033193 -0.029862
 -0.026058 -0.021945 -0.017726 -0.013595 -0.009463 -0.005225 -0.001094
    F
 0.006032 0.012488 0.015727 0.018285 0.020444 0.026978 0.034727
                                                                    0.040687
 0.045100 0.048900 0.052100 0.055103 0.057433 0.059633 0.061791
                                                                    0.065792
 0.068588 0.070417 0.071149 0.071025 0.069806 0.067614 0.064577
                                                                    0.060598
 0.055848 0.050013 0.042853 0.034400 0.024790 0.013589 0.001108
 0.006032 -0.003871 -0.007209 -0.009141 -0.010737 -0.015212 -0.020623 -0.024567
```

```
-0.027415 -0.029582 -0.031085 -0.032517 -0.033762 -0.034738 -0.035713 -0.037375
-0.038636 -0.039376 -0.039394 -0.038/90 -0.037429 -0.035359 -0.032617 -0.029446
-0.025451 -0.021305 -0.017055 -0.012808 -0.008666 -0.004766 -0.001108
 0.049100 0.052765 0.055845 0.058205 0.060562 0.062634 0.064687
                                                                      0.068398
 0.071018 0.071863 0.071501 0.069947
                                         0.067091 0.063104 0.058319
                                                                      0.052545
 0.045971 0.038907 0.031906 0.024620 0.017412 0.009606 0.001006
 0.000745 -0.002368 -0.006812 -0.009262 -0.011326 -0.016277 -0.020702 -0.023207
 -0.024618 -0.025424 -0.025906 -0.026314 -0.026715 -0.027243 -0.027735 -0.029567
 -0.032057 -0.034703 -0.036336 -0.036447 -0.035379 -0.033157 -0.029948 -0.026146
-0.021978 -0.017757 -0.012968 -0.008576 -0.004595 -0.002006 -0.001006
*** END OF C5 AIRFOIL DATA ***
C5 PLANFORM DESCRIPTION
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         0.0
                   79.21
                             178.80
                                        94.36
                                                 123.36
18720.0
         221.36
                   55.34
        2
        2
0.0
         0.0
                   82.0
                             44.14
.538292683.538292683
82.0
         44.14
                   178.80
                             94.36
.518801653.518801653
        2
         79.21
0.0
                   82.0
                             93.21
.170731707.170731707
82.0
          93.21
                   178.80
                             123.36
.311466942.311466942
                                       .458612975 2.68
0.0
         4.18
                   .388702461 2.9
                                                           .604026846 2.18
1.0
          -0.9
26X30X8 MESH
&GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0, NTIPLE=1&END
 &XGRID NXON=10, NXFWD=8, NXAFT=8, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=1.5&END
 &ZGRID NZ=8,ZP=3.3&END
 &SOLVIN MACH=.775, AOA=2.00, MAXIT=220, OMEGX=1.92,
        OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=220,
        OMEGZ=1.92, CON=1.0, NGSEQ=3, BXI=0.0,
        IPLOT=0, IPU=8, OMEGG=1.2, IKLUNK=0, IDESN=0&END
 45X30X16 MESH
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1.ISHEAR=0, NTIPLE=1&END
 &XGRID NXON=25, NXFWD=10, NXAFT=10, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=1.5&END
 &ZGRID NZ=16, ZP=1.75, ZMAX=5.0&END
 &SOLVIN MAXIT=300, OMEGX=1.92,
        OMEGY=1.92, RCONV=.0001.IPRINT=0, ICIRPF=300, NITRL=100, NJSHP=4,
        OMEGZ=1.92,CON=1.0,IPRSHP=0,IRLOFT=3,
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# IPLOT=0,IPU=8,OMEGG=1.2,IKLUNK=0,IDESN=2,ILED=16,NITRF=10, ITED=35,NITDSN=50,ISVSHP=1,IINV=1,IVISC=0&END

C5 INV MOD 4 LINEAR CP RECOVERY J=1-19 1 19 50 0.010101 0.030303 0.050505 0.070707 0.090909 0.111111 0.131313 0.151515 0.171717 0.191919 0.212121 0.232323 0.252525 0.272727 0.292929 0.313131 0.333333 0.353535 0.373737 0.393939 0.414141 0.434343 0.454545 0.474747 0.494949 0.515152 0.535354 0.555556 0.575758 0.595960 0.616162 0.636364 0.656566 0.676768 0.696970 0.717172 0.737374 0.757576 0.777778 0.797980 0.818182 0.838384 0.858586 0.878788 0.898990 0.919192 0.939394 0.959596 0.979798 1.000000 0.250413 -0.547996 -0.690000 -0.750000 -0.770000 -0.790000 -0.800000 -0.790000 -0.780000 -0.760000 -0.720000 -0.680000 -0.620000 -0.560000 -0.480000 -0.440000 -0.350000 -0.260000 -0.160000 -0.040000 0.065930 0.179936 0.345951 0.010101 0.030303 0.050505 0.070707 0.090909 0.111111 0.131313 0.191919 0.212121 0.151515 0.171717 0.232323 0.252525 0.272727 0.292929 0.313131 0.333333 0.353535 0.373737 0.393939 0.414141 0.535354 0.434343 0.454545 0.474747 0.494949 0.515152 0.555556 0.575758 0.595960 0.616162 0.636364 0.656566 0.676768 0.696970 0.717172 0.737374 0.757576 0.777778 0.797980 0.818182 0.838384 0.939394 0.858586 0.878788 0.898990 0.919192 0.959596 0.979798 1.000000 -0.133011 -0.834330 -0.865831 -0.850000 -0.830000 -0.800000 -0.790000 -0.770000 -0.740000 -0.700000 -0.670000 -0.610000 -0.550000 -0.500000 -0.420000 -0.350000 -0.250000 -0.160000 -0.090000 0.020967 0.103324 0.210316 0.358176 0.010101 0.070707 0.090909 0.131313 0.030303 0.050505 0.111111 0.151515 0.171717 0.191919 0.212121 0.232323 0.252525 0.272727 0.292929 0.313131 0.333333 0.353535 0.373737 0.393939 0.414141 0.434343 0.454545 0.474747 0.494949 0.515152 0.535354 0.555556 0.575758 0.595960 0.616162 0.636364 0.656566 0.676768 0.696970 0.717172 0.737374 0.757576 0.777778 0.797980 0.818182 0.838384 0.858586 0.878788 0.898990 0.919192 0.939394 0.959596 0.979798 1.000000 -0.301318 -0.944470 -1.040394 -0.930000 -0.850000 -0.820000 -0.800000 -0.770000 -0.770000 -0.750000 -0.720000

```
-0.680000 -0.640000 -0.590000 -0.540000 -0.470000 -0.400000 -0.350000
-0.280000 -0.200000 -0.130000 -0.060000 0.032365 0.113458
0.361156
0.010101
          0.030303 0.050505
                              0.070707
                                         0.090909
                                                   0.111111
0.151515
           0.171717
                    0.191919
                              0.212121
                                         0.232323
                                                   0.252525
                                                             0.272727
0.292929
           0.313131
                     0.333333
                               0.353535
                                         0.373737
                                                   0.393939
                                                             0.414141
0.434343
           0.454545
                     0.474747
                               0.494949
                                         0.515152
                                                   0.535354
                                                             0.555556
0.575758
           0.595960
                     0.616162
                               0.636364
                                         0.656566
                                                   0.676768
                                                             0.696970
0.717172
           0.737374
                     0.757576
                               0.777778
                                         0.797980
                                                   0.818182
0.858586
           0.878788
                     0.898990
                               0.919192
                                         0.939394
                                                   0.959596
1.000000
-0.417676 -1.013660 -1.122306 -1.085846 -0.994702 -0.877198 -0.800000
-0.800000 -0.800000 -0.800000 -0.800000 -0.800000 -0.800000 -0.800000
-0.800000 -0.800000 -0.800000 -0.800000 -0.800000 -0.800000 -0.800000
-0.800000 -0.800000 -0.800000 -0.800000 -0.800000 -0.800000
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-0.640000 -0.600000 -0.540000 -0.490000 -0.430000 -0.390000 -0.320000
-0.240000 -0.170000 -0.100000 -0.020000 0.039454 0.119653 0.222646
0.363919
0.010101
           0.030303 0.050505
                              0.070707
                                         0.090909
                                                   0.111111
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 0.717172 0.737374 0.757576 0.777778 0.797980 0.818182 0.838384
 0.858586 0.878788 0.898990 0.919192 0.939394 0.959596 0.979798
 1.000000
-0.789175 - 1.184176 - 1.268442 - 1.315068 - 1.351130 - 1.346501 - 1.335827
-1.312219 -1.276365 -1.245651 -1.220000 -1.210000 -1.200000 -1.200000
-1.200000 -1.200000 -1.200000 -1.200000 -1.200000 -1.200000
-1.200000 -1.200000 -1.200000 -1.200000 -1.170000 -1.110000
-1.040000 -0.974283 -0.908566 -0.842848 -0.777131 -0.711414 -0.645697
-0.579979 -0.514262 -0.448545 -0.382828 -0.317111 -0.251394 -0.185677
-0.119959 -0.054242 0.011475 0.077192 0.142909 0.208627 0.274344
0.340061
 0.010101 0.030303 0.050505 0.070707 0.090909 0.111111 0.131313
0.151515 0.171717 0.191919 0.212121 0.232323 0.252525 0.272727
```

```
0.292929 \quad 0.313131 \quad 0.333333 \quad 0.353535 \quad 0.373737 \quad 0.393939 \quad 0.414141
0.555556
0.575758 0.595960 0.616162 0.636364 0.656566 0.676768 0.696970
0.717172 0.737374 0.757576 0.777778
                                       0.797980 0.818182 0.838384
0.858586 0.878788 0.898990 0.919192 0.939394 0.959596 0.979798
1.000000
-0.789175 -1.184176 -1.268442 -1.315068 -1.351130 -1.346501 -1.335827
-1.312219 -1.276365 -1.245651 -1.220000 -1.210000 -1.200000 -1.200000
-1.200000 -1.200000 -1.200000 -1.200000 -1.200000 -1.200000
-1.200000 -1.200000 -1.200000 -1.200000 -1.200000 -1.170000 -1.110000
-1.040000 -0.974283 -0.908566 -0.842848 -0.777131 -0.711414 -0.645697
-0.579979 -0.514262 -0.448545 -0.382828 -0.317111 -0.251394 -0.185677
-0.119959 -0.054242 0.011475 0.077192 0.142909 0.208627 0.274344
0.340061
 TRAILING EDGE THICKNESS TARGETS
 19
0.002
          0.002
                    0.002
                              0.002
                                        0.002
                                                 0.002
                                                           0.002
                    0.002
0.002
          0.002
                              0.002
                                        0.002
                                                  0.002
                                                           0.002
0.002
          0.002
                    0.002
                              0.002
                                        0,002
90X30X30 GRID
&GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0&END
&XGRID NXON=50, NXFVD=20, NXAFT=20&END
&YGRID NYON=20, NYOFF=10, YMAX=1.5&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=300.OMEGX=1.90,NITRL=20,NITRF=40,
        OMEGY=1.90, RCONV=.001, IPRINT=1, ICIRPF=300, ISVSHP=1,
        OMEGZ=1.90, IPLOT=1, IPU=8, OMEGG=1.2, IKLUNK=0, ISRLOR=1,
        BXI=0.0,CON=1.0,ILED=31,ITED=70,NITDSN=1,IPRSHP=0&END
```

# SAMPLE DATA SET NO. 3 RAE WING BODY TEST CASE

RAE WING A WING BODY TEST CASE MACH=0.80 AOA=2.0
RAE WING "A" ORDINATES

IGIL WING	n ONDINA	125					
2	86	86	0				
0.000000	0.001000	0.002000	0.003000	0.004000	0.005000	0.006000	0.007000
0.007500	0.008000	0.009000	0.010000	0.012000	0.012500	0.014000	0.016000
0.018000	0.020000	0.025000	0.030000	0.035000	0.040000	0.050000	0.060000
0.070000	0.075000	0.080000	0.090000	0.100000	0.120000	0.140000	0.150000
0.160000	0.180000	0.200000	0.220000	0.240000	0.250000	0.260000	0.280000
0.300000	0.320000	0.340000	0.350000	0.360000	0.380000	0.400000	0.420000
0.440000	0.450000	0.460000	0.480000	0.500000	0.520000	0.540000	0.550000
0.560000	0.580000	0.600000	0.620000	0.640000	0.650000	0.660000	0.680000
0.700000	0.720000	0.740000	0.750000	0.760000	0.780000	0.800000	0.820000
0.840000	0.850000	0.860000	0.880000	0.900000	0.920000	0.925000	0.940000
0.950000	0.960000	0.975000	0.980000	0.987500	1.000000		
0.000000	0.001000	0.002000	0.003000	0.004000	0.005000	0.006000	0.007000
0.007500	0.008000	0.009000	0.010000	0.012000	0.012500	0.014000	0.016000
0.018000	0.020000	0.025000	0.030000	0.035000	0.040000	0.050000	0.060000
0.070000	0.075000	0.080000	0.090000	0.100000	0.120000	0.140000	0.150000
0.160000	0.180000	0.200000	0.220000	0.240000	0.250000	0.260000	0.280000
0.300000	0.320000	0.340000	0.350000	0.360000	0.380000	0.400000	0.420000
0.440000	0.450000	0.460000	0.480000	0.500000	0.520000	0.540000	0.550000
0.560000	0.580000	0.600000	0.620000	0.640000	0.650000	0.660000	0.680000
0.700000	0.720000	0.740000	0.750000	0.760000	0.780000	0.800000	0.820000
0.840000	0.850000	0.860000	0.880000	0.900000	0.920000	0.925000	0.940000
0.950000	0.960000	0.975000	0.980000	0.987500	1.000000		
0.000000	0.003515	0.004966	0.006078	0.007013	0.007835	0.00 <b>857</b> 6	0.009256
0.009578	0.009888	0.010480	0.011039	0.012074	0.012318	0.013022	0.013901
0.014721	0.015494	0.017257	0.018832	0.020262	0.021577	0.023903	0.026008
0.027863	0.028722	0.029540	0.031067	0.032466	0.034938	0.037046	0.037982
0.038847	0.040380	0.041674	0.042746	0.043610	0.043966	0.044271	0.044730
0.044972	0.044960	0.044752	0.044582	0.044376	0.043855	0.043205	0.042438
0.041565	0.041091	0.040595	0.039539	0.038403	0.037196	0.035924	0.035265
0.034592	0.033209	0.031779	0.030308	0.028803	0.028039	0.027267	0.025707
0.024126	0.022531	0.020926	0.020121	0.019317	0.017707	0.016097	0.014487
0.012878	0.012073	0.011268	0.009658	0.008049	0.006439	0.006036	0.004829
0.004024	0.003219	0.002012	0.001610	0.001006	0.000000		
0.000000	-0.003515	-0.004966	-0.006078		-0.007835	-0.008576	
-0.009578	-0.009888	-0.010480			-0.012318	-0.013022	
-0.014721			-0.018832		-0.021577	-0.023903	
-0.027863			-0.031067				
-0.038847			-0.042746				
-0.044972	-0.044960	-0.044752	-0.044582	-0.044376	-0.043855	-0.043205	-0.042438

```
-0.041565 -0.041091 -0.040595 -0.039539 -0.038403 -0.037196 -0.035924 -0.035265
-0.034592 -0.033209 -0.031779 -0.030308 -0.028803 -0.028039 -0.027267 -0.025707
-0.024126 -0.022531 -0.020926 -0.020121 -0.019317 -0.017707 -0.016097 -0.014487
-0.012878 -0.012073 -0.011268 -0.009658 -0.008049 -0.006439 -0.006036 -0.004829
-0.004024 -0.003219 -0.002012 -0.001610 -0.001006 0.000000
*** END OF RAE AIRFOIL DATA ***
RAE WING PLANFORM DESCRIPTION
                                         11.160306 14.160306
0.0
          0.0
                     8.0
                               15.0
          5.5
                     7.208
82.5
         1
         2
                     15.0
                               11.160306
          0.0
0.0
.744020
          .744020
         1
         2
                               14.160306
                     15.0
0.0
          8.0
          .410946
.410946
                               0.0
                     1.0
0.0
          0.0
 26X30X8
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0, NTIPLE=1&END
 &XGRID NXON=10, NXFVD=8, NXAFT=8, XFVD=-5.XAFT=8.0&END
 &YGRID NYON=20.NYOFF=10.YMAX=1.4&END
 &ZGRID NZ=8,ZP=3.3&END
 &SOLVIN MACH=0.80, AOA=2.0, MAXIT=400, OMEGX=1.92,
          OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=100,
          OMEGZ=1.92.CON=1.0,NGSEQ=3.BXI=0.0,NF=30,
          IPLOT=0.IPU=8.OMEGG=1.2.IKLUNK=1.IFUSE=2&END
                                  RBODY
                                            LENGTH
                                                       ALF
                       ZBODY
             YBODY
  XBODY
                                            70.
                                                       16.
                                  3.0
                       0.
  22.232
             3.
  NST
   20
             AREA
   XF
           0.0
   0.0
   2.0
           2.58155
   4.0
           8.33570
           14.87571
    6.0
           20.62897
   8.0
           24,78582
   10.0
           27.18065
   12.0
   14.0
           28.13185
           28.27433
   16.0
           28.27433
   22.0
   28.0
           28.27433
           28.27433
   32.0
           28.27433
   36.0
   40.0
           28.27433
   45.95
           28.27433
           21.64754
```

47.0

```
48.0
         15.90431
49.0
         11.04466
50.0
         7.06858
70.
         3.14159
45X30X16 GRID
&GPARM IPRNTG=0.WBCPRT=.F.&END
&XGRID NXON=25, NXFVD=10, NXAFT=10&END
&YGRID NYON=20, NYOFF=10, YMAX=1.4, RTSWCH=1.0&END
&ZGRID NZ=16,ZMAX=5.0&END
&SOLVIN MAXIT=400, OMEGX=1.9,
        OMEGY=1.9.RCONV=.0001,ICIRPF=100,
        OMEGZ=1.9&END
90X30X30 GRID
&GPARM IPRNTG=O&END
&XGRID NXON=50.NXFVD=20.NXAFT=20&END
&YGRID NYON=20.NYOFF=10,YMAX=1.4&END
&ZGRID NZ=30&END
&SOLVIN MAXIT=100, OMEGX=1.9,
        OMEGY=1.9, RCONV=.001, IPRINT=1, ICIRPF=50,
        OMEGZ=1.9, IPLOT=1, IPU=8, OMEGG=1.2, IKLUNK=1&END
```

### SAMPLE DATA SET NO. 4 F14 INVISCID ANALYSIS

F14 INVISCID ANALYSIS WITH BOPPE CODE ORDINATES 2 GRIDS MACH =  $.8\ AOA=1.4$ 

	BAOA=1.4						
		GRUMMAN RI	EPORT				
9	50	50	0				
0.000000	0.001910	0.004960	0.009950	0.020000	0.039930	0.060000	0.080000
0.100000	0.120000	0.140000	0.160000	0.180000	0.200000	0.220000	0.240000
0.260000	0.280000	0.300000	0.320000	0.340000	0.360000	0.380000	0.400000
0.420000	0.440000	0.460000	0.480000	0.500000	0.520000	0.560000	0.600000
0.640000	0.680000	0.700000	0.720000	0.740000	0.760000	0.780000	0.800000
0.820000	0.840000	0.860000	0.880000	0.900000	0.920000	0.940000	0.960000
0.980000	1.000000						
0.000000	0.001910	0.004960	0.009950	0.020000	0.039930	0.060000	0.080000
0.100000	0.120000	0.140000	0.160000	0.180000	0.200000	0.220000	0.240000
0.260000	0.280000	0.300000	0.320000	0.340000	0.360000	0.380000	0.400000
0.420000	0.440000	0.460000	0.480000	0.500000	0.520000	0.560000	0.600000
0.640000	0.680000	0.700000	0.720000	0.740000	0.760000	0.780000	0.800000
0.820000	0.840000	0.860000	0.880000	0.900000	0.920000	0.940000	0.960000
0.980000	1.000000						
0.004660	0.010460	0.014220	0.018540	0.025040	0.034540	0.041700	0.047300
0.051770	0.055340	0.058180	0.060420	0.062140	0.063440	0.064370	0.064990
0.065330	0.065430	0.065320	0.065020	0.064560	0.063950	0.063200	0.062320
0.061330		0.059030	0.057730	0.056350	0.054870	0.051650	0.048100
0.044240		0.037880	0.035610	0.033280	0.030880	0.028420	0.025900
0.023320		0.018000	0.015280	0.012510	0.009710	0.006880	0.004030
	-0.001710						
		-0.005400					
		-0.036060					
		-0.039400					
		-0.034680					
		-0.022720					
		-0.014470	-0.013470	-0.012480	-0.011500	-0.010520	-0.009550
	-0.007610						
T F							
0.007560		0.017100	0.021010	0.026720	0.034850	0.040950	0.045820
0.049830	0.053170	0.055960	0.058270	0.060170	0.061700	0.062910	0.063810
0.064440		0.064960	0.064890	0.064620	0.064160	0.063520	0.062710
0.061750	0.060640	0.059380	0.058000	0.056480	0.054850	0.051240	0.047220
0.042840	0.038120	0.035660	0.033130	0.030540	0.027900	0.025210	0.022470
0.019700	0.016890	0.014050	0.011190	0.008300	0.005400	0.002490	-0.000430
	-0.006280						_
0.007560	0.001820				-0.015670		
	-0.025320				-0.029320		
-0.030870	-0.031200	-0.031440	-0.031600	-0.031680	-0.031690	-0.031630	-0.031500

```
-0.031300 \ -0.031050 \ -0.030730 \ -0.030360 \ -0.029930 \ -0.029450 \ -0.028340 \ -0.027060
-0.025620 -0.024050 -0.023220 -0.022360 -0.021480 -0.020580 -0.019660 -0.018720
-0.017770 -0.016800 -0.015820 -0.014840 -0.013850 -0.012850 -0.011850 -0.010850
 -0.009840 -0.008840
    F
 0.008780 0.014880 0.018310 0.022050
                                          0.027420 0.034980
                                                              0.040630 0.045190
 0.049010 0.052260 0.055020 0.057370
                                          0.059340 0.060970
                                                              0.062290 0.063310
 0.064060
           0.064560
                     0.064810 0.064830
                                          0.064640
                                                    0.064240
                                                              0.063650
                                                                        0.062880
 0.061930
           0.060810 0.059530 0.058110
                                                              0.051070
                                          0.056540
                                                    0.054840
                                                                        0.046850
 0.042240
           0.037300 0.034730
                               0.032090
                                          0.029390
                                                    0.026650
                                                              0.023860 0.021030
 0.018180 0.015290 0.012390 0.009470
                                          0.006530
                                                    0.003590 0.000640 -0.002310
 -0.005260 -0.008210
 0.008780 0.003240 -0.000230 -0.003620 -0.007780 -0.012730 -0.015890 -0.018190
 -0.019970 -0.021420 -0.022630 -0.023660 -0.024550 -0.025340 -0.026040 -0.026650
 -0.027200 -0.027670 -0.028080 -0.028430 -0.028710 -0.028930 -0.029090 -0.029180
 -0.029200 \ -0.029170 \ -0.029070 \ -0.028900 \ -0.028680 \ -0.028390 \ -0.027650 \ -0.026680
-0.025520 -0.024170 -0.023430 -0.022660 -0.021850 -0.021000 -0.020130 -0.019230
 -0.018310 -0.017360 -0.016390 -0.015410 -0.014420 -0.013420 -0.012410 -0.011390
 -0.010370 -0.009350
T
     F
 0.007220
           0.013270 0.016570 0.020330
                                          0.025640 0.033000
                                                              0.038520 0.043010
 0.046820
           0.050100 0.052940 0.055400
                                          0.057510
                                                    0.059300
                                                              0.060780 0.061980
 0.062910 0.063590 0.064020 0.064210
                                          0.064190
                                                    0.063950
                                                              0.063510 0.062870
           0.061050 0.059890
 0.062050
                                0.058560
                                          0.057080
                                                    0.055460
                                                              0.051820
                                                                        0.047700
 0.043170
           0.038280
                                                    0.027700
                      0.035720
                                0.033100
                                          0.030420
                                                              0.024920 0.022110
 0.019270
           0.016400 0.013510 0.010610
                                          0.007700 0.004780
                                                              0.001850 -0.001070
 -0.004000 -0.006920
 0.007220 \quad 0.001650 \quad -0.001730 \quad -0.005030 \quad -0.008970 \quad -0.013570 \quad -0.016500 \quad -0.018630
 -0.020290 -0.021640 -0.022770 -0.023750 -0.024610 -0.025370 -0.026060 -0.026680
 -0.027230 -0.027720 -0.028160 -0.028530 -0.028840 -0.029090 -0.029280 -0.029400
 -0.029450 -0.029440 -0.029360 -0.029210 -0.029000 -0.028710 -0.027950 -0.026940
 -0.025700 \ -0.024240 \ -0.023430 \ -0.022580 \ -0.021680 \ -0.020740 \ -0.019770 \ -0.018760
 -0.017720 -0.016650 -0.015560 -0.014450 -0.013320 -0.012170 -0.011020 -0.009860
 -0.008690 -0.007530
     F
 0.003160
           0.009280 0.012600 0.016420
                                          0.021800 0.029280 0.034900 0.039490
  0.043410
           0.046820 0.049810 0.052430
                                          0.054720
                                                    0.056710
                                                              0.058400
                                                                        0.059820
                                                              0.063040
 0.060980
           0.061890 0.062560
                                0.063010
                                          0.063230
                                                    0.063240
                                                                        0.062650
 0.062070
           0.061310 0.060380
                                0.059280
                                          0.058020
                                                    0.056620
                                                              0.053380
                                                                        0.049640
                                0.035980
  0.045450
           0.040870
                     0.038460
                                          0.033420
                                                    0.030810
                                                              0.028150
                                                                        0.025440
 0.022700
           0.019920 0.017120 0.014300
                                          0.011460 0.008610 0.005750
                                                                        0.002900
 0.000040 -0.002820
  0.003160 \ -0.002590 \ -0.005810 \ -0.009040 \ -0.012920 \ -0.017390 \ -0.020190 \ -0.022200 
 -0.023750 -0.025010 -0.026060 -0.026960 -0.027750 -0.028440 -0.029060 -0.029620
 -0.030100 -0.030520 -0.030880 -0.031170 -0.031390 -0.031550 -0.031630 -0.031640
 -0.031580 -0.031440 -0.031230 -0.030940 -0.030570 -0.030140 -0.029050 -0.027680
 -0.026050 -0.024180 -0.023160 -0.022090 -0.020970 -0.019800 -0.018590 -0.017340
 -0.016060 -0.014740 -0.013400 -0.012030 -0.010640 -0.009230 -0.007810 -0.006380
 -0.004940 -0.003500
```

```
F
T
 -0.002100 \quad 0.004120 \quad 0.007540 \quad 0.011340 \quad 0.016800 \quad 0.024410 \quad 0.030160 \quad 0.034880
            0.042490 0.045650 0.048450 0.050940 0.053140 0.055070
  0.038930
                                                                          0.056750
  0.058170 0.059360 0.060320 0.061060 0.061580 0.061890 0.062000
                                                                          0.061910
  0.061640 0.061180 0.060540 0.059740 0.058770 0.057650 0.054960
                                                                          0.051730
  0.048020 0.043880 0.041680 0.039390 0.037020 0.034580 0.032090
                                                                          0.029540
  0.026940 0.024310
                      0.021640 0.018940 0.016230 0.013490 0.010750 0.008000
  0.005250 0.002490
 -0.002100 -0.007870 -0.011230 -0.014270 -0.017990 -0.022260 -0.024900 -0.026740
 -0.028140 \ -0.029260 \ -0.030190 \ -0.030980 \ -0.031670 \ -0.032270 \ -0.032800 \ -0.033250
 -0.033630 \ -0.033950 \ -0.034190 \ -0.034360 \ -0.034460 \ -0.034470 \ -0.034410 \ -0.034260
  -0.034040 \ -0.033730 \ -0.033340 \ -0.032860 \ -0.032300 \ -0.031670 \ -0.030150 \ -0.028330 
 -0.026220 \ -0.023840 \ -0.022560 \ -0.021220 \ -0.019820 \ -0.018370 \ -0.016870 \ -0.015320
 -0.013740 \ -0.012110 \ -0.010460 \ -0.008770 \ -0.007060 \ -0.005330 \ -0.003580 \ -0.001830
 -0.000060 0.001710
     F
                                                                          0.028650
 -0.009190 -0.003000 0.000610 0.004520 0.010080 0.017870 0.023780
  0.032870 0.036590 0.039930 0.042940 0.045660 0.048100 0.050300
                                                                          0.052260
                                           0.058760 0.059440 0.059920
  0.053990 0.055500
                      0.056790 0.057880
                                                                          0.060220
  0.060330 0.060260
                      0.060010 0.059600
                                           0.059020 0.058280 0.056340
                                                                          0.053840
                                           0.041390 0.039230 0.037000
  0.050830 0.047350
                      0.045450
                                0.043470
                                                                          0.034710
  0.032350 0.029940 0.027490 0.025000 0.022490 0.019940 0.017380 0.014810
  0.012230 0.009650
 -0.009190 -0.014990 -0.018310 -0.021310 -0.024870 -0.028830 -0.031180 -0.032780
 -0.033960 \ -0.034880 \ -0.035630 \ -0.036260 \ -0.036790 \ -0.037220 \ -0.037580 \ -0.037860
 -0.038060 -0.038180 -0.038220 -0.038180 -0.038050 -0.037840 -0.037530 -0.037150
 -0.036670 -0.036100 -0.035450 -0.034700 -0.033870 -0.032960 -0.030870 -0.028460
 -0.025730 -0.022720 -0.021110 -0.019430 -0.017690 -0.015900 -0.014040 -0.012140
 -0.010190 \ -0.008200 \ -0.006170 \ -0.004100 \ -0.002010 \ \ 0.000110 \ \ 0.002250 \ \ 0.004400
  0.006560 0.008730
 -0.019120 -0.012950 -0.009370 -0.005400 0.000370 0.008440 0.014560 0.019630
  0.024040 0.027960 0.031510 0.034740 0.037710 0.040430 0.042930
                                                                          0.045210
  0.047290 0.049170 0.050850 0.052350
                                           0.053660 0.054790 0.055740
                                                                          0.056520
  0.057120 0.057550 0.057810 0.057910
                                           0.057850 0.057640 0.056760
                                                                          0.055310
  0.053330 0.050870 0.049470 0.047960 0.046350 0.044660 0.042870
                                                                          0.041010
  0.039080 0.037080 0.035030 0.032920 0.030780 0.028600 0.026390
                                                                          0.024160
  0.021920 0.019680
 -0.019120 \ -0.025250 \ -0.028510 \ -0.031390 \ -0.034700 \ -0.038160 \ -0.040020 \ -0.041170
 -0.041950 -0.042510 -0.042930 -0.043220 -0.043420 -0.043530 -0.043540 -0.043470
 -0.043320 \  \, -0.043080 \  \, -0.042750 \  \, -0.042340 \  \, -0.041840 \  \, -0.041250 \  \, -0.040580 \  \, -0.039820
 -0.038970 \ -0.038030 \ -0.037000 \ -0.035880 \ -0.034680 \ -0.033380 \ -0.030540 \ -0.027350
 -0.023850 -0.020030 -0.018010 -0.015920 -0.013760 -0.011540 -0.009260 -0.006920
 -0.004520 -0.002080 0.000400 0.002920 0.005480 0.008060 0.010670 0.013290
  0.015920 0.018560
     F
 -0.034510 -0.028160 -0.024430 -0.020280 -0.014350 -0.005910 0.000530
                                                                          0.005870
  0.010530 0.014700 0.018500 0.022000 0.025250 0.028270 0.031090
                                                                          0.033730
  0.036180 0.038470 0.040600 0.042560 0.044370 0.046020 0.047520 0.048870
```

```
0.050070 0.051120 0.052020 0.052780 0.053400 0.053880 0.054440
                                                                         0.054490
 0.054050 0.053170 0.052570 0.051870 0.051070 0.050190 0.049230
                                                                         0.048200
 0.047090 0.045920 0.044700 0.043430 0.042120 0.040780 0.039410
 0.036620 0.035210
 -0.034510 -0.040970 -0.044000 -0.046630 -0.049350 -0.051350 -0.051670 -0.051490
 -0.051150 -0.050760 -0.050360 -0.049950 -0.049510 -0.049030 -0.048510 -0.047930
 -0.047290 -0.046580 -0.045800 -0.044950 -0.044010 -0.042990 -0.041870 -0.040670
 -0.039380 -0.037990 -0.036500 -0.034920 -0.033240 -0.031470 -0.027630 -0.023410
 -0.018840 \ -0.013920 \ -0.011350 \ -0.008690 \ -0.005970 \ -0.003170 \ -0.000310 \ \ 0.002610
 0.005580 0.008590 0.011660 0.014750 0.017880 0.021040 0.024210 0.027400
  0.030600 0.033800
         END OF AIRFOIL DATA ***
     F14 PLANFORM DESCRIPTION
0.0
          0.0
                    167.20971 384.69995 140.06494 184.32837
40676.853 160.0
                    76,00073
         1
         2
0.0
          0.0
                    384.69995 140.06494
.364088792.364088792
         1
          167.20971 384.69995 184.32837
.047914841.047914841
                                                                         0.0
0.0
          0.0
                    .330725
                               0.0
                                         .42634
                                                    0.0
                                                              .52196
.61758
                                         .80882
                                                             .90444
                                                                         0.0
          0.0
                    .71320
                               0.0
                                                    0.0
1.0
           0.0
 45X30X16 MESH
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, ISHEAR=0, NTIPLE=1&END
 &XGRID NXON=25, NXFWD=10, NXAFT=10, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=2.0&END
 &ZGRID NZ=16, ZP=1.75, ZMAX=5.0&END
 &SOLVIN MACH=.80, AOA=1.4, NGSEQ=2, MAXIT=300, RCONV=.001,
         OMEGX=1.80, OMEGY=1.80, OMEGZ=1.80, OMEGG=1.2,
         IPRINT=0, IPLOT=0, ICIRPF=100, IKLUNK=1,
         CON=1.0.BXI=0.0&END
 90X30X30 MESH
 &GPARM IPRNTG=0&END
 &XGRID NXON=50.NXFVD=20,NXAFT=20&END
 &YGRID NYON=20, NYOFF=10&END
 &ZGRID NZ=30&END
 &SOLVIN MAXIT=300, RCONV=.001, IPRINT=1, IPLOT=1, ICIRPF=300,
         OMEGX=1.8, OMEGY=1.8, OMEGZ=1.8, OMEGG=1.2&END
```

### SAMPLE DATA SET NO. 5 WING A VISCOUS ANALYSIS

```
WING A VISCOUS ANALYSIS
 MACH=0.80 AOA=1.2
 WINGA ORDINATES
        2
                 33
                           33
 0.000000
                     0.009607 0.021530
                                                0.059039 0.084265
           0.002408
                                       0.038060
                                                                     0.113495
                     0.222215
                              0.264302
                                                                     0.450991
  0.146447
           0.182803
                                        0.308658
                                                 0.354858
                                                           0.402455
                              0.645142
 0.500000
           0.549009
                     0.597545
                                        0.691342
                                                  0.735698
                                                           0.777785
                                                                     0.817197
  0.853553
           0.886505
                     0.915735
                              0.940961
                                        0.961940
                                                  0.978470
                                                           0.990393
                                                                     0.997592
  1.000000
  0.000000 0.002408
                     0.009607
                              0.021530
                                        0.038060
                                                 0.059039
                                                           0.084265
                                                                     0.113495
  0.146447
           0.182803
                     0.222215
                              0.264302
                                        0.308658
                                                           0.402455
                                                 0.354858
                                                                     0.450991
  0.500000
           0.549009
                     0.597545
                              0.645142
                                        0.691342
                                                 0.735698
                                                           0.777785
                                                                     0.817197
  0.853553
           0.886505
                     0.915735
                              0.940961 0.961940
                                                 0.978470
                                                           0.990393
                                                                     0.997592
  1.000000
  0.000000 0.009523
                     0.017576 0.024310 0.030180
                                                 0.034958
                                                           0.038571
                                                                     0.041361
  0.043645 0.045539
                     0.047036 0.048065 0.048637
                                                  0.048737
                                                           0.048351
                                                                     0.047358
  0.045740 0.043449
                     0.040624
                              0.037256
                                        0.033534
                                                  0.029576
                                                           0.025544
                                                                     0.021533
           0.014102 0.010867 0.008059 0.005745
  0.017667
                                                 0.003816 0.002366
                                                                     0.001245
  0.000801
 0.000000 -0.007998 -0.015781 -0.022051 -0.028216 -0.034320 -0.040552 -0.046841
 -0.053095 -0.058886 -0.063909 -0.067723 -0.070312 -0.071256 -0.070937 -0.068816
 -0.065403 -0.060078 -0.053487 -0.045480 -0.036948 -0.028384 -0.020344 -0.013234
 -0.007335 -0.002835 0.000160 0.001680 0.001953 0.001417 0.000485 -0.000425
 -0.000803
    F
  0.000000 0.007883 0.016974 0.025572 0.033052
                                                 0.039841
                                                           0.046100 0.051716
          0.060668 0.064013
                              0.066654
                                       0.068589
                                                  0.069825
                                                           0.070362
                                                                     0.070214
  0.069431
           0.067991
                     0.065908
                              0.063109
                                        0.059558
                                                  0.055045
                                                           0.049478
                                                                    0.042953
 0.035847 0.028744 0.022061
                                                 0.007448 0.004805
                              0.016177 0.011340
                                                                    0.002848
  0.002073
  0.000000 -0.008988 -0.015880 -0.021410 -0.025889 -0.029641 -0.033196 -0.036588
 -0.039898 -0.042959 -0.045616 -0.047750 -0.049215 -0.049918 -0.049642 -0.048016
 -0.044596 -0.039227 -0.032380 -0.024781 -0.017099 -0.009966 -0.003808 0.000991
          0.004231
 -0.002070
*** END OF WINGA AIRFOIL DATA ***
WINGA PLANFORM DESCRIPTION
         0.0
                              18.00000 9.36853
                     6.500
                                                 11.96853
81.8
         4.825
                   5.221
        1
        2
0.0
         0.0
                   18.000
                              9.36853
.520474
         .520474
```

```
2
0.0
                                 11.96853
          6.5
                     18.000
.303808
          .303808
0.0
          2.57
                     1.0
                                -2.00
 25X30X8 GRID
 &GPARM IPRNTG=0, WBCPRT=.F., ISAMG=1, NTIPLE=1&END
 &XGRID NXON=10, NXFWD=7, NXAFT=8, XFWD=-5.0, XAFT=8.0&END
 &YGRID NYON=20, NYOFF=10, YMAX=2.0&END
 &ZGRID NZ=8, ZP=3.3&END
 &SOLVIN MACH=0.80, AOA=1.2, MAXIT=400, OMEGX=1.92,
         OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=100,
         OMEGZ=1.92,CON=1.0,NGSEQ=3,BXI=0.0,
         IPLOT=0, IPU=8.OMEGG=1.2, IKLUNK=1, IDESN=0&END
 45X30X16 GRID
 &GPARM IPRNTG=0, WBCPRT=.F.&END
 &XGRID NXON=25, NXFWD=10, NXAFT=10&END
 &YGRID NYON=20.NYOFF=10&END
 &ZGRID NZ=16.ZP=1.75,ZMAX=5.0&END
 &SOLVIN MAXIT=400, OMEGX=1.95, OMEGY=1.95, RCONV=.0001, IPRINT=0,
         ICIRPF=100, OMEGZ=1.95, CON=1.0, BXI=0.0, IVISC=1,
         IPLOT=0, IPU=8, OMEGG=1.2&END
 &VISCDT ITR=10, NVISC=100, NPRV=401, NJPRV=9, RN=8080000.,
         DELCOR=.82139&END
 90X30X30 GRID
 &GPARM IPRNTG=0, WBCPRT=.F.&END
 &XGRID NXON=50, NXFWD=20, NXAFT=20&END
 &YGRID NYON=20, NYOFF=10&END
 &ZGRID NZ=30&END
 &SOLVIN MAXIT=400, OMEGX=1.95,
         OMEGY=1.95, RCONV=.0001, IPRINT=1, ICIRPF=50,
         OMEGZ=1.95, IPLOT=1, IPU=8, OMEGG=1.2, IKLUNK=1,
         BXI=0.0, CON=1.0&END
 &VISCDT ITR=10, NVISC=100, NPRV=400, NJPRV=9&END
```

## SAMPLE DATA SET NO. 6 WING C INVISCID ANALYSIS

```
WING C INVISCID ANALYSIS
MACH=0.83 AOA=5.0
WING C ORDINATES
                 33
                           33
 0.000000
           0.002408 0.009607
                               0.021530 0.038060 0.059039
                                                            0.084265
 0.146447
           0.182803
                     0.222215
                               0.264302
                                        0.308658 0.354858
                                                            0.402455
                                                                      0.450991
 0.500000
           0.549009
                     0.597545
                               0.645142
                                        0.691342
                                                            0.777785
                                                  0.735698
                                                                      0.817197
 0.853553
           0.886505
                     0.915735
                               0.940961
                                         0.961940 0.978470
                                                            0.990393
                                                                      0.997592
 1.000000
 0.000000 0.002408
                     0.009607
                               0.021530
                                       0.038060 0.059039
                                                            0.084265
                                                                      0.113495
 0.146447
           0.182803
                     0.222215
                               0.264302
                                        0.308658
                                                  0.354858
                                                            0.402455
                                                                      0.450991
 0.500000
          0.549009
                     0.597545
                               0.645142
                                        0.691342 0.735698
                                                            0.777785
                                                                      0.817197
 0.853553
           0.886505
                     0.915735
                               0.940961
                                        0.961940 0.978470
                                                            0.990393
                                                                      0.997592
  1.000000
 0.000000 0.007078 0.015211
                               0.022409 0.028113 0.032665
                                                            0.036344
                                                                      0.039106
 0.040977
          0.042046
                    0.042446
                               0.042381
                                         0.041875 0.040963
                                                            0.039692
 0.036025
           0.033750
                     0.031266
                               0.028567
                                         0.025780 0.022922
                                                            0.020008
                                                                      0.017060
 0.014113
           0.011218 0.008528 0.006165 0.004213 0.002720
                                                            0.001669 0.001034
 0.000820
 0.000000 - 0.006221 - 0.009909 - 0.012680 - 0.015584 - 0.018603 - 0.021094 - 0.023104
 -0.024642 -0.025693 -0.026348 -0.026447 -0.026081 -0.025220 -0.024010 -0.022330
 -0.020180 -0.017188 -0.013545 -0.009434 -0.005720 -0.002752 -0.000712 0.000412
 -0.000823
    F
 0.000000 0.005979 0.014276 0.022373 0.030131 0.037796 0.045339
                                                                      0.052724
                               0.078516 0.082519 0.084923
 0.059929 0.066822 0.073148
                                                            0.085600
                                                                      0.084549
 0.081909 0.077914
                     0.072839
                               0.066913
                                        0.060301
                                                  0.053236
                                                            0.046023
                                                                      0.038892
 0.032028
           0.025650 0.019838
                               0.014702 0.010355 0.006916
                                                            0.004546 0.003161
 0.002704
 0.000000 - 0.008265 - 0.012773 - 0.015803 - 0.018133 - 0.020204 - 0.021813 - 0.023033
 -0.023855 - 0.024169 - 0.024120 - 0.023592 - 0.022620 - 0.021102 - 0.019120 - 0.016540
 -0.013462 -0.009562 -0.005017 -0.000128  0.004105  0.007319  0.009262  0.009845
 0.009212 \quad 0.007659 \quad 0.005620 \quad 0.003410 \quad 0.001300 \quad -0.000327 \quad -0.001630 \quad -0.002422
 -0.002681
*** END OF WING C AIRFOIL DATA ***
WINGC PLANFORM DESCRIPTION
0.0
                   12.140
                             10.26000 10.26000 13.90
         0.0
81.0
         8.642
                   6.367
        1
         2
0.0
         0.0
                   10.260
                             10.26
```

```
1.0
          1.0
0.0
          12.14
                     10.260
                               13.90
.171539961.171539961
          2.39
0.0
                               -5.59
                     1.0
 26X30X8 GRID
 &GPARM WBCPRT=.F.,NTIPLE=1&END
 &XGRID XFVD=-5.0, XAFT=8.0, NXON=10, NXFVD=8, NXAFT=8&END
 &YGRID NYON=20, NYOFF=10, YMAX=1.4&END
 &ZGRID NZ=8, ZP=3.3&END
 &SOLVIN MACH=0.83.AOA=5.0, MAXIT=400, OMEGX=1.92, IKLUNK=1,
         OMEGY=1.92,RCONV=.00001,IPRINT=0,ICIRPF=100,
         OMEGZ=1.92,NGSEQ=3,IPLOT=0,IPU=8,OMEGG=1.2&END
 45X30X16 GRID
 &GPARM WBCPRT=.F.&END
 &XGRID NXON=25.NXFWD=10,NXAFT=10&END
 &YGRID NYON=20, NYOFF=10&END
 &ZGRID NZ=16, ZMAX=5.0&END
 &SOLVIN MAXIT=400, OMEGX=1.9, OMEGY=1.9, RCONV=.0001,
         IPRINT=1, ICIRPF=100, OMEGZ=1.9&END
 90X30X30 GRID
 &GPARM IPRNTG=0, VBCPRT=.F.&END
 &XGRID NXON=50, NXFVD=20, NXAFT=20&END
 &YGRID NYON=20, NYOFF=10&END
 &ZGRID NZ=30&END
 &SOLVIN MAXIT=100, OMEGX=1.75, OMEGY=1.75, RCONV=.001,
         IPRINT=1,ICIRPF=50,OMEGZ=1.75,IPLOT=1&END
```

# APPENDIX B SAMPLE OUTPUT

The following pages illustrate the major blocks of data that are printed during the course of an analysis or design run.

TEST CASE DESCRIPTION

シングの自然をあることも自然ななななない。というなどのなっては自己というなどのない。

H6 VISCOUS INV VISC TARG WITH HODIFIED CPS 45 12 JD 12,12 ZEBIPLS VERS OF CODE CORRECTED SHAPE DIEW . OI MAXIT 400

... AIRFOIL ORDINATES INPUT FROM UNIT 5 ...

... END OF SECTION DATA ....

ONERA H6 PLANFORN DESCRIPTION

YHOM XLER XTER YTIP XLET XTET 0 0000 805 90001196 3000 690 68411143 5999 YROOT 0 0000

NLES

NLEI

DXLER DXLET 0 577350 0.577350

NTES

NTEI

YTEI XTEI 0.0000 805.9000 1196.3000 1143.5999

DXTER DXTET 0.282971

KSMTHS 0 1NU 69 NPAN 4

THETP(N)
0.000000
0.000000
0.000000 YP(N) 0.000000 0.200000 0.600000 0.899880

PLANFORM INPUT DESCRIPTION

		o		000000						
							00100			
_							210010			0.024107
	-			621860 0	0.065630	<b>o</b>	200820	0.080.0		028411 0
_						۰ د	00.11.2			
_						0	478120			
_	0 577804	0			٠.	0	675273		ກ	
~	0 220800	0	794106	0 817483	0.840732	0	863856	•	Ę,	
_	0.936335	0	847895	0.957851	0 966186	0	973236	D.979202	ď	0.984251
-	0.992144	0	. 995208	0 997803	1.000000					
_	WHICH LOWER	WER	SURFACE	ORDINATES	ARE INPUT					
_	0.000323	0		0.000866	0.001287	0	001836	0.002544		0.003443
_	0 005975	0	007711	0.009841	0 012448	0	015617	0.019461	_	0.024107
_		0		0 054125	0 065630	0	079337	0.095635		0.114980
_	0.164998	0	191933	0.218710	0.245331	0	271798	0.298111	_	0.324273
•	0 376145				0.452844	0	478120	0.503251		0.528243
•	0.577804	0		0.626810	0.651109	0	675273	0 699303	_	0.723199
_	0.770600	0	794106	0.817483	0 840732	0	863856	0.886823	E)	0.906191
_		0		0.957851		၁	973236		Q	0.984251
_					1.000000					
				9						
	THE FOLLOWING Z	20								
				0.005134		Ö	0.007478	0.008798		
-	0.013371			0.016898			020622	0.022455		
_	0.027332	0		0.030328	0.032014	0	033837	0.035774	4	0.037792
_	0.041909	0	043621	0.045051	0.046236	0	0.047199	0.047949	0	0.048490
_	0.048930	0	048820	0.048483	0.047935	Ö	.047166	0.046190		0.045021
_	0.042168	0	.040524	0.038761	0.036899	Ö	.034954	0.032940	0	0.030866
	0.026550	0	024303	0.021984	0.019584	Ö	017091	0.014505	ŝ	0.012239
	0.008583	0	007142	0.005922	0.004891	0	004018	0.003280	2	0.002655
	0.001678	0		0.000977	0.000705					
	THE FOLLOWING 2	21 C	ARE INPUT	TO						
	0.003138	-	.004096	0.005134	0.006260	Ö	007478	0.008796		0 010216
	0.013371	0	.015095	0.016898	0.018754	0	020622	0.022455		0.024200
	0.027332	0	028791	0.030328	0.032014	0	033837	0.035774	-	0.037792
	0 041909	0	043621	0 045051	0.046236	0	047199	0.047949		0.048490
	0.048930	0	048820	0.048483	0.047935	0	047166	0.046190		0.045021
-	0.042168	0		0.038761		0	034954		_	0.030866
	_	-		0.021984	0.019584		017091		-	
				00800	004400		910400			

■日からのののは豊間できたのでの機能である。ためる機能である。このではない機能である。

AIRFOIL SECTION ORDINATES

COARSE SKEWED MESH

シン 全層 はれたのこととは 層層なれたこれの 色層の こうこう 引き間

XPIE 0.2000	
XPLE 0.2000	
NXAFT	YPT IP
8	1 3000
NXFWD	NYOFF
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NXON	NYON
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( 192, OMEGY 192, OMEGZ 1.92, NI 90, NJ 30, NK 30, RCONV 1.E5, IPRINI 0. IPLOT 0. ISDBC 0, NDIF 0. IFUSE 0. NITRL 100, SRHAX 1.00, IPRSHP 0. IRLOFT 0. IVISC 0. ICPSDC 0. OMEGG 1.2, ICIRPF 100 1.00, ILED 0. ITED 0. NITDSN 0. ISVSHP 0. INV 0. IRSTRI 0. NF HEND #SOLVIN HAXIT 200 ONEGX AOA 3 06 HACH 0 8395 CON 1 IDESN 0 IOPT NGSEQ 3 IPU 8 NITRE ISRLOR 0 IPSHPF 100 W

O. O227 CPU SECONDS INPUT REQUIRED

> 1 585522 XPLE XP

1.860146 XPTE 1.241286

MESH GENERATION DATA

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SWEEP	SWEEP	CHORD	CHORD	AREA.	RATIO	RATIO	CHORD
0 5774		1 0000	0 5620	1 159	3 8014	0 5620	0 8017
	DNIM	LEADING AND TRAILING EDGE COORDINATES	TRAILING	EDGE COOL	RDINATES		
	ETA	XLEW	XIEW	33			
NOHINAL	WING ROOT						
	0.00000.0	0 000000	~	000000			
	0 076124	0 043950	7	021533			
	0.152249	0 087901	7	043052			
	0 228373	0 131851	~	064558			
	0.304498	0 175802	-	086054			
	0.380622	0 219752	-	107539			
	0 456747	0 263703	-	129017			
	0 532871	0.307653	1.1	150489			
	0.608996	0.351604	7	171956			
	0.685120	0 395554	1 1	193420			
	0.781245	0.439505	-	214883			
	0.837369	0 483455	7	236346			
	0.913494	0.527406	7	257812			
	0.989618	0.571356	7	279281			
	1 065743	0 615307	-	300756			
	1 141867	0.659257	-	322237			
	1 217992	0 703208	-	343727			
	1.294116	0.747158	-	365228			
	1 370241	0 791109		386740			

¥	ETA	XLE	XTE	XIEP	XTEP
NOMINAL	WING ROOT				
7	0.00000	0 000000	1 000000	0 577350	0.282971
œ	0.076124	0 043950	1.021533	0 577350	0.282772
8	0 152249	0 087901	1.043052	0 577350	0.282593
4	0.228373	0 131851	1.064558	0 577350	0 282437
S	0 304498	0 175802	1.086054	0 577350	0.282302
9	0 380822	0 219752	1 107539	0 577350	0 282188
t-	0 456747	0 263703	1 129017	0 577350	0.282097
89	0 532871	0 307853	1.150489	0.577350	0.282026
ø	966809 0	0 351604	1 171958	0 577350	0 281978
10	0.685120	0.395554	1.193420	0.577350	0.281951
11	0.761245	0.439505	1.214883	0.577350	0 281945
12	0 837369	0 483455	1.236346	0.577350	0 281962
13	0.913494	0.527406	1.257812	0 577350	0.281999
14	0.989618	0.571356	1.279281	0.577350	0.282059
15	1.085743	0 615307	1.300756	0.577350	0.282140
16	1 141867	0.659257	1.322237	0 577350	0.282242
17	1.217992	0.703208	1 343727	0.577350	0.282367
18	1.294116	0 747158	1.365228	0.577350	0.282512
61	1.370241	0.791109	1.386740	0 577350	0.282680

# COMPUTED PLANFORM DATA

0 282869				0 577350	0 577350	0.577350	0.577350	0.577350	0 577350	0 577350	0 577350		בי אה																						
0.527350		0.577350	0.527350	0.527350	0 577350	0 577350	0 577350	0.577350	0.577350	0 577350	0 577350	;	EDGE FOINTS AND I	(X XTEW) C		1 000000	1 0000000	1 000000	1 000000	1.000000	1.000000	1.000000	1.000000	000000	000000	1.000000	1 0000000	1.000000	1.000000	1 000000	1.000000	1.000000	000000	000000	<b>1</b> .000000
1 408266		1 429805	1 473756	1 528311	1 596029	1 680087	1 784427	1.913943	2.074710	2 274267	2 521975		LEADING AND TRAILING	(X XLEW) C		0.052632	0 052632	0 052632	0.052632	0.052632	0.052632	0 052632	0.052632	0 052632	0.052632	0.052632	0 052632	0 052632	0.052632	- 7.	0 052632	0 052632			0.052632
0.835059		010628 0	0 922960	0 977515	1 045234	1 129292	1 233632	1 363148	1 523915	1 723472	1 971179		INDEX OF LEADIN	JLE JIE		8 17	8 17	8 17	8 17	8 17	8 17	8 17	8 17	8 17	8 17	8 17	8 17	7	8 17		8 17	8 12	8 17	8 17	8 12
	L WING TIP	1 522490	1 598614	1 693106	1 810398	1 955991	2 136714	2.361042	2 639498	2 985141	3 414183		2	ETA	WING ROOT	0000000	0 076124	0 152249	0.228373	0.304498	0 380622	0 456747	0.532871	966809 0	0 685120	0 761245	0 837369	0 913494	0 989618	1 065743	1 141867	1 217992	1.294116	1 370241	1.446385
೧೫	NOMINAL	12	828	53	2.4	25	56	27	28	58	30			×	NOMINAL	-	O)	က	4	ഗ	ø	٥	<b>3</b> 0	<b>3</b> 3	10	11	12	13	14	15	16	1.7	18	16	50

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0.11502 CPU SECONDS

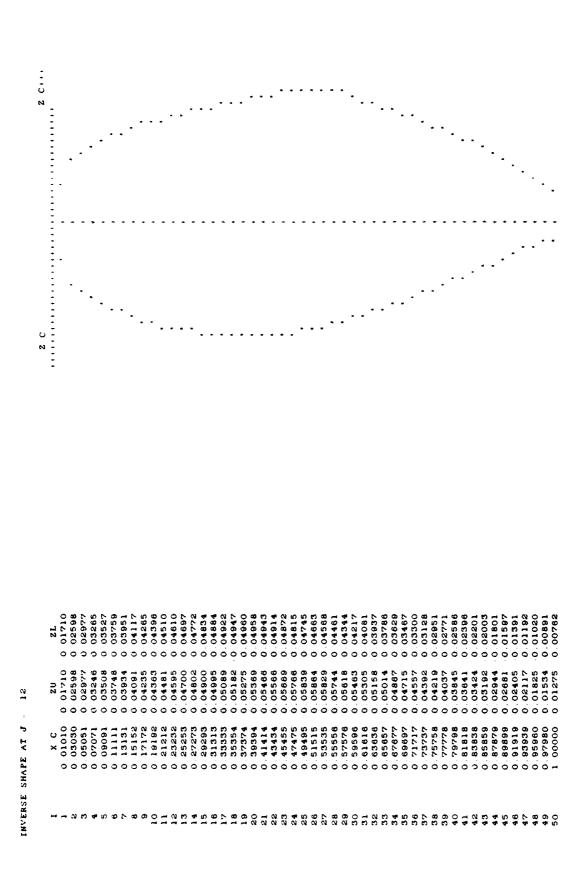
HESH GENERATION REQUIRED

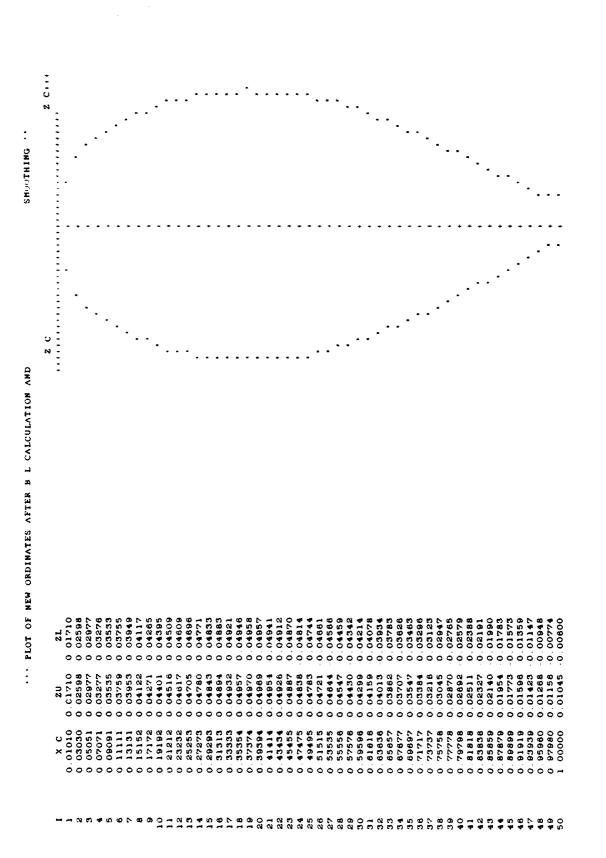
0.0016 CPU SECONDS

INITIALIZATION REQUIRED

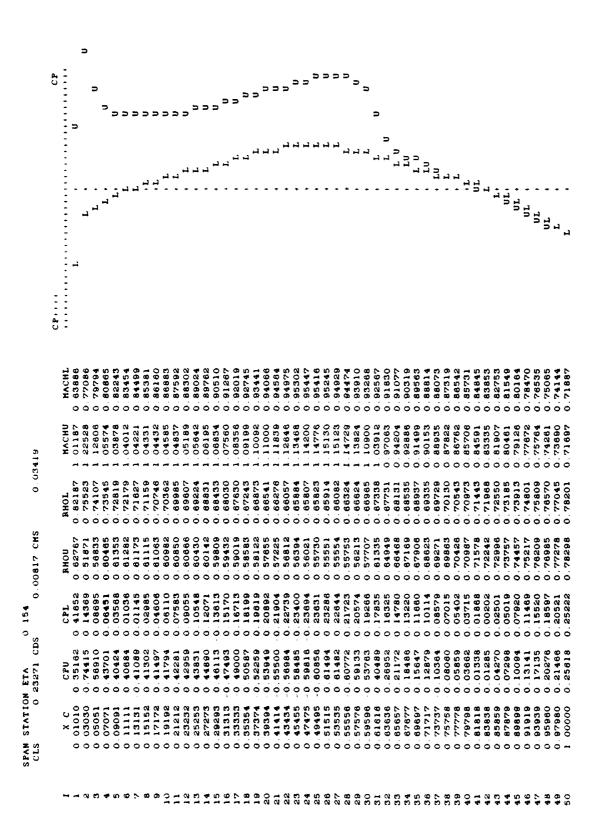
	10	03	10	10	10	01	10	01	01	10	<b>6</b> ;	10	7 7	7 6	3 6	; ;	;	: 6	010	01	10	-01	01	01	0,	010	, 10:	<b>7</b>	10	0	0.0	<b>7</b> 6	5 6			-01	10	010	6	3 3	3 6	3 3	5 6	3 6	2 0	3 0	3 0	3 0	2 C	2 0	1
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X	-		3 0		13710E	1055E	8331	69460			. 50970E	0.48117E+00	٠.		0.37850E+00	00.386838.0	00.10000000				30		0.27814E:00	. 2662				0.22114E+00	œ	. 39	0.18647E+00	٠,	0.16825E+00		1 4	7	7	_	_	7.		100455	95024E	SOCKE	- 1000000	O. SIADOR OI	77159E	300827	0.687415-01	ALEGE E	- TCZCTO.
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2	CHAN	10000	113301	2	300016		40189F	41465E	39641E	63	8	28202E	32721E	.26567E	19872E	18454E	.25184E	E SUBSERIE	0.155765-02	147875	189165	16307E	13613E	13361E	13043E	14550E	11998E	11477E	10906E	-	98559E	93741E	88986E		80066E	72497E	68784E	85278E	62291E	59298E	. 56300E	53342E	50441E	47925E	.45563E-0	43239E 0	40948E	SHEROF O	36450E 0	34148	32527E-0
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	BOUNDARY	BUUNDARY LAYER ANALYSIS FOR REYNOLDS NO	SIS	FOR REY	NOLDS NO	OF 0 205E.08	E,08						
×	2	ZNEW		r	DELS	THETA	SEP	I		PI	ONI		TAU
0 07071	0 03271		-	30845		0 00001	c 00000	1.04530	- 0	16664	13	000	00186
0 09091	0 03524	0 03535	_	17606	0.00012	90000 0	0.00013	2 01341	0.1	0.13480	12	00 0	00161
0 11111	0 03741	0 03759	-	13413	0.00019	0 00010	0.00005	1.90857	00	02334	=	00 0	00154
0 13131	0.03929	0.03953	-	13903	0 00024	0.00013	0.00004	1.87177	Õ.	06475	11	0.00	00148
0 15152	0.04093	0.04122	_	14959	0 00029	0 00016	0.00009	1.86620	0	05075		00 0	00143
0 17172	0.04236	0.04271	~	15635	0.00034	0.00018	0 00003	1.86617	ö	03483	7.7	0.00]	00138
0.19192	0 04362	0.04401	, ,	16024	0.00039	0.00021	0.00002	1.86456	0.0	03207	11	0.00]	00134
0.21212	0.04472	0.04516	-	16334	0.00044	0.00024	0.00003	1.86153	ŏ.	04057	10	0.00	00132
0.23232	0.04568	0 04617	~	16680	0.00048	0.00028	0.00003	1.85837	0.0	05684	10	0.001	00130
0.25253	0.04652	0.04705	_	17118	0.00053	0 00029	0.00005	1.85592	0.0	07727	01	0.00	00128
0.27273	0 04723	0.04780	-	17661	0 00057	0.00031	90000.0	1.85469	0.0	09782	01	00.0	00126
0.29293	0 04782	0 04843	-	18298	0.00061	0.00033	0.00007	1.85476	0	11918	01	0.001	00125
0.31313	0.04828	0.04894	-	19023	0.00065	0.00035	6000000	1.85608	0	13871	10	0.00	00124
0.33333	0.04863	0.04932	~	19816	0.00069	0.00037	0.00010	1.85877	0	15337	01	0 00	00123
0 35354	0 04884	0.04957	~	20647	0.00073	0.00039	0.00011	1.86245	0	16818	10	0.001	00122
0.37374	0 04893	0.04970	-	21513	0.00077	0.00041	0.00011	1.86724	.10	17265	01	0.00121	181
0 39394	0.04888	0.04969	~	22360	0.00081	0.00043	0.00010	1 87474	ò	14048	01	0.00	00119
0 41414	0.04868	0 04954	-	23011	0 00085	0.00045	0.00007	1 88489	0	07593	10	00 0	00116
0 43434	0.04835	0.04926	-	23340	0.00089	0.00047	0.00002	1.89619	0	02778	10	0 O	00113
0.45455	0 04789	0.04887	-	23228	0.00095	0.00050	0.00007	1.90983	0	21881	10	00 0	60100
0 47475	0 04728	0.04838	-	22439	0.00101	0.00052	0.00025	1 93689	0	75195	10	000	00100
0.49495	0.04653	0.04783	-	20191	0.00115	0 00056	0.00081	2.04031	3	53550	13	000	00074
0 51515	0.04566	0.04721	_	14015	0.00154	0.00065	0.00195	2 38170	25.5	57653	38	0 0	000027
0.53535	0.04465	0.04644	-	04230	0.00202	0.00084	0.00234	2 41017	Š.	54940	17	0000	00052
0.55556	0.04353	0.04547	0	90286	0.00190	0.00098	0.00114	1 94222	÷	44129	*	0 00	66400
0.57576	0.04230	0.04430	o	98095	0.00174	0.00101	0.00034	1,71521	0	79443	2	000	\$6000
0 59596	0.04097	0.04299	Ö	97114	0.00184	0.00106	0.00055	1.74422	-	33751	10	) ) 0	000087
	0.03954	0.04159	0	92696	0.00195	0.00111	0.00069	1.75935	<del>-</del>	46372	7	000	98000
	0.03804	0.04013	0	94275	0.00205	0.00117	0.00071	1 75054	<del>¥</del> ~	13767	11	0 000	000086
0 65657	0.03647	0.03862	Ö	92963	0.00213	0 00123	0.00071	1 73777	7	13954	Ξ.	000	00085
	0.03483	0.03707	Ö	91731	0.00222	0 00159	0.00072	1 72926	2	50647	Ξ.	0 0	000184
	0.03314	_	Ö	90529	0.00232	0 00135	0.00075	1.72478	ĕ -	60696	:	ŏ0 0	00083
	0.03139	0.03384	Ö	89341	0.00243	0 00141	0 00078	1 72224	- 2	72473	11	00 o	00081
	0 02960	0.03216	Ö	88161	0.00254	0 00147	0 00085	1 72235	š	90457	11	0.00	08000
	0.02776		0	86965	0 00288	0.00154	0 00098	1 78501	3	11718	11	000	00078
	0 02587	0 02870	0	85751	0.00279	0 00162	66000 0	1 72897	ei ei	33511	=	÷000	0CO 26
	0 02392	0.02692	0	84529	0.00294	0.00169	0 00108	1 73695	C.	71361	=	000	00073
	0.02191		Ö	83259	0.00313	0.00178	0 00124	1 76052	e e	54300	75	٥ ٥	000088
	0.01983	0.02327	Ö	81851	0.00339	0.00188	0 00120	1 80529	ð	94413	13	300	00061
	0 01767	0.02140	Ö	80273	0 00368	0 00500	0 00172	1 84548	ès O	87518	13	300	00:057
	0.01542	0.01954	Ö	78685	0.00394	0.00213	0.00181	1.85461	9	03249	12	0.000	00056
	0.01309	0.01773	o	77203	0.00429	0.00226	0.00203	86006 1	6	40472	18	00 0	000148
	0.01068	0.01596	Ö	75551	0.00534	0.00242	0.00875	2 20735		92064	55	000	51000
	0.00821	0 01423	0	73394	0.00621	0.00268	0 00307	2 31573	22	15929	88	000	00028
0 95960	0.00571	0.01268	Ö	71711	0.00555	0.00290	0.00205	1.91248	œ N	96701	11	0000	00008
0.97980	0.00321	0.01156	ó	71048	0.00733	0.00299	0.00265	2.44948*	:	::	51	0.000	00000
1.00000	0.00070	0.01045	Ö	0.69042	0.01012	0.00339	0.00552	2.98649	:	::	51	0.0000.0	000





VISCOUS AIRFOIL PRINTER PLOT



WING SECTION PRESSURE COEFFICIENT PRINTER PLOT AND DATA TABULATION

### REFERENCES

1. South, J. C., Keller, J. D., and Hafez, M., "Vector Processor Algorithms for Transonic Flow Calculations," AIAA Journal, Vol. 18, No. 7, 1980 pp. 786-792.

# -IMED 4-86